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# FINAL REPORT 250 kV ELECTRON GUN

JANUARY 1986

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U.S. NAVAL RESEARCH LABORATORY  
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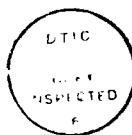
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Two high-voltage, high-power Pierce-type electron guns were designed and developed for use at the NRL high-power ubitron laboratory. The design of the high-voltage and vacuum housings of the guns incorporates design features utilized in the SLAC XK-5 klystron gun. Detail design data and beam trajectories are presented. Beam analyzer and high voltage tests are discussed. Assembly and detail drawings are included.		

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## 1.0 INTRODUCTION

### 1.1 PURPOSE

The purpose of this program was to develop a high-voltage, high-power Pierce-type electron gun to be used for experiments at the NRL high-power ubitron laboratory. These experiments are intended for high-power, high-quality electron-beam generation, beam diagnostics, and high-power microwave generation techniques.

### 1.2 SCOPE

In accordance with Contract No. N00014-85-C-2059 two electron guns were fabricated, pretested and delivered to NRL. The high-voltage and vacuum housings of the guns were consistent with the design utilized in the Stanford Linear Accelerator Center (SLAC) XK-5 klystron gun. This 12-month development program covers the period from December 1984 through December 1985.

The report describes details of beam optics calculations, performance characteristics, pretest results, and includes assembly and detail drawings along with a material list.

## 2.0 CALCULATIONS AND COMPUTED RESULTS

### 2.1 DIODE CHARACTERISTICS AND ELECTRON TRAJECTORIES

The process of arriving at optimum electron beam trajectories involves an iterative computational procedure and computer graphics plotting. Repetitive testing in the Varian computer controlled beam analyzer, to confirm the desired results, is limited to lower voltages (20 kV to 25 kV). Finalized electrostatic beam trajectories are illustrated in Figure 1 and Figure 2 for 20 kV and 250 kV respectively.

### 2.2 MAGNETIC FIELD

In the case of a confined-flow focusing system the magnetic field at the cathode can be determined approximately from the following expression:

$$B_c = \frac{(B_o)(\alpha)}{(r_c/r_o)^2} \text{ gauss}$$

where:  $B_c$  = Magnetic Field at Cathode  
 $B_o$  = Main Field  
 $r_c$  = Radius of Cathode  
 $r_o$  = Radius of Beam  
 $\alpha$  = Cathode Flux Parameter

The mathematical expression for calculating is as follows:

$$\alpha = \sqrt{1 - \left(\frac{B_{br}}{B_o}\right)^2}$$

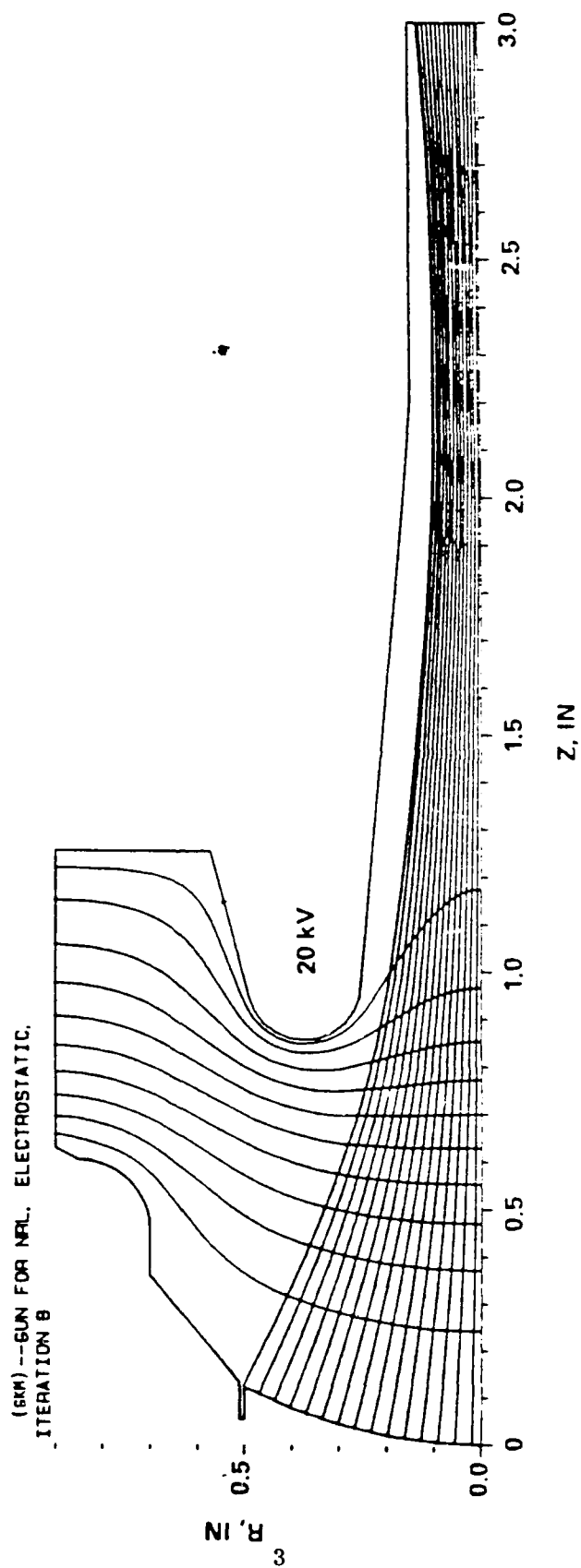


FIGURE 1. NONRELATIVISTIC BEAM TRAJECTORIES (20 kV)

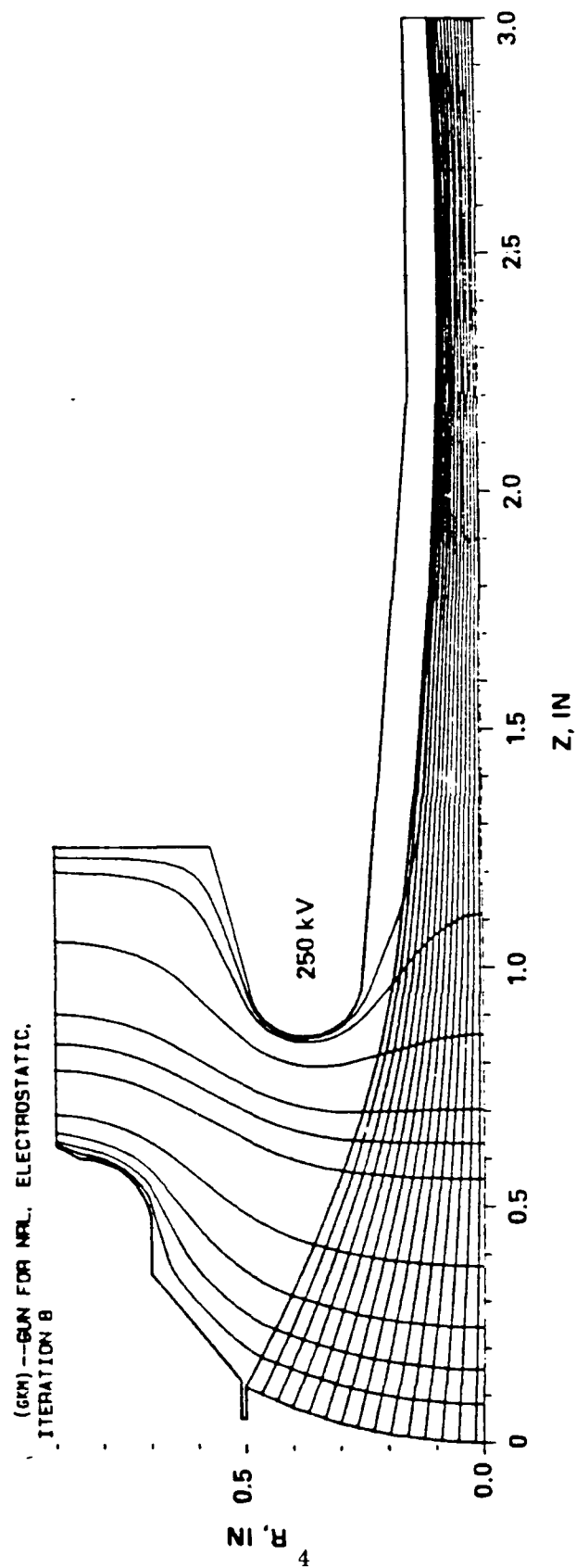


FIGURE 2. RELATIVISTIC BEAM TRAJECTORIES (250 kV)



where:  $B_{br}$  is the Brillouin field value and is equal to

$$B_{br} = \frac{463.5 \text{ (V) (k)}}{d} \quad (\text{For Low Beam Voltages})$$

$$= \left( \frac{468}{d} \right) \cdot \mu^{1/2} \left[ \frac{\left( 1 + \frac{V_o}{2 \times 510.98} \right)^{1/2}}{\frac{V_o}{510.98}} \right]^{1/2} \text{Field} \quad \text{Relativistically Corrected } B_{BR}$$

where:  $\mu$  = Microperveance  
 $V_o$  = Beam Voltage in kV

where:  $d$  = Beam Diameter (inches)  
 $V$  = Beam Voltage  
 $k$  = Perveance

The design magnetic field is calculated from these expressions and is plotted in Figure 3. (Relativistic)

### 2.3 COMPUTER GUN OPTICS DESIGN

With the aid of the Varian computer gun design programs, several designs were generated and analyzed. The gun electrode geometries were optimized in order to achieve the desired beam characteristics and voltage gradients around the focus electrode anode areas. Aside from determining the required perveance, convergence and voltage gradients, special attention was given to produce an extremely laminar beam in order to obtain the minimum axial velocity spread. In the final design, the velocity spread was computed to be 0.295%. Details of computer calculations were described in detail in previous reports.

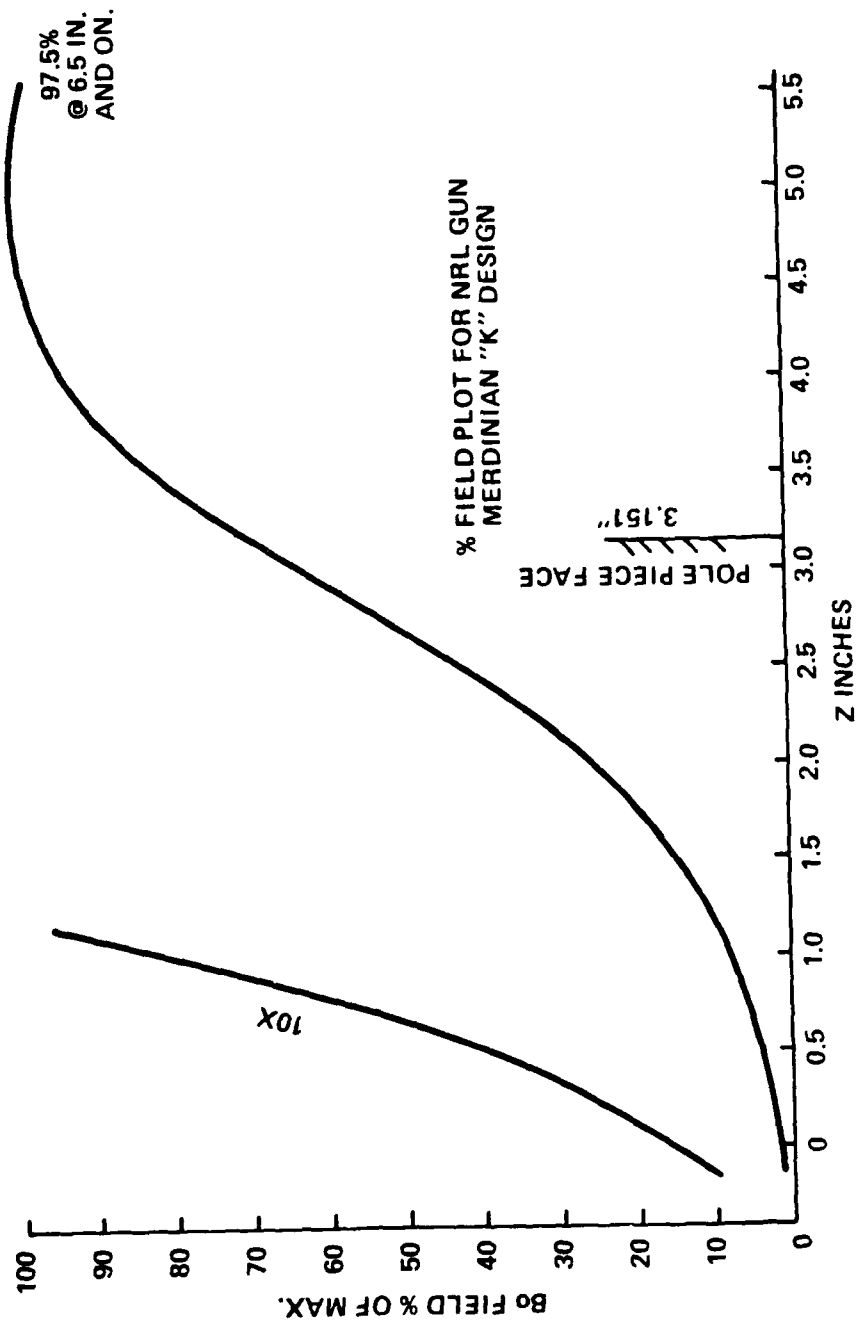


FIGURE 3. % MAGNETIC FIELD vs DISTANCE FROM CATHODE

In order to test the gun in the beam analyzer the tests can only be made at maximum voltage of 20 kV. The magnetic field was correspondingly adjusted.

### 3.0 DESIGN METHODOLOGY

The design and development of this electron gun followed a procedure which defines a certain sequence of events as described below:

1. A detailed computer analysis of the Pierce-type diode gun was performed at two beam voltages of 20 kV and 250 kV.
2. The beam trajectories in a confined-flow magnetic focusing field were calculated and plotted by the computer for 20 kV and 250 kV as illustrated in Figure 4 and Figure 5 respectively.
3. In order to ensure the integrity of the design at high-voltage operation, a computer plot of the voltage gradient in vacuum was generated as shown in Figure 6.
4. The electrostatic beam optics were then evaluated in a computer-controlled beam analyzer and the configuration refined for optimum performance.
5. Subsequently, the electron gun was placed in a confined-flow magnetic focusing field and retested. Reiterative modifications to the magnetic focusing field were introduced until satisfactory results were obtained.

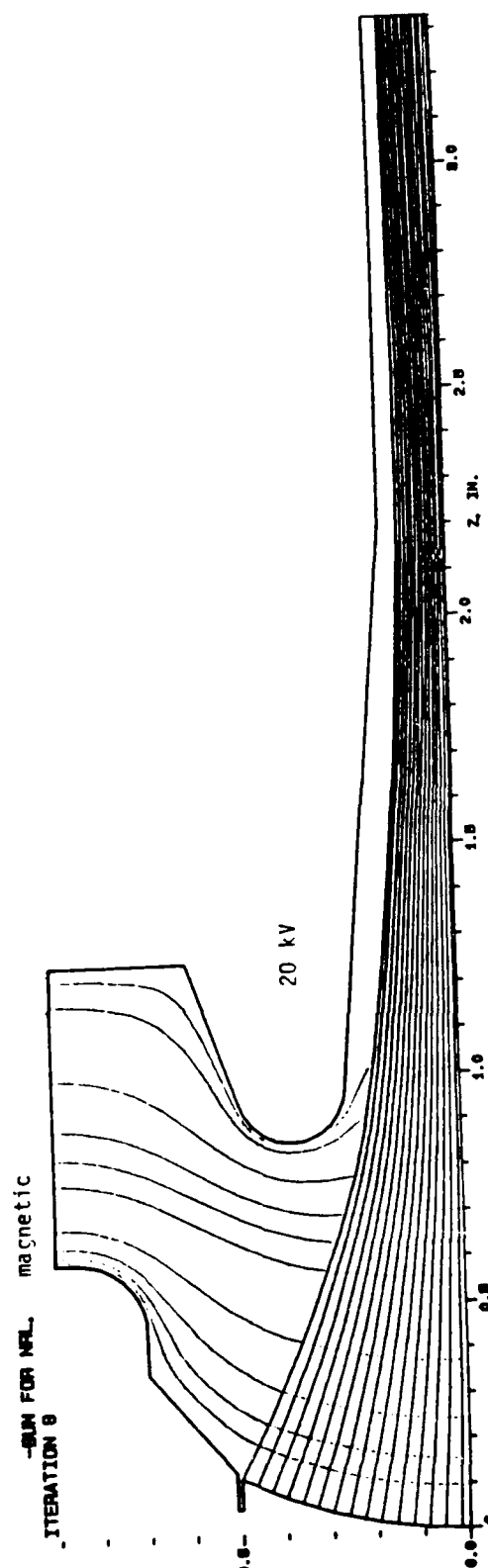


FIGURE 4. BEAM TRAJECTORIES IN CONFINED-FLOW MAGNETIC FOCUSING FIELD (20 kV)

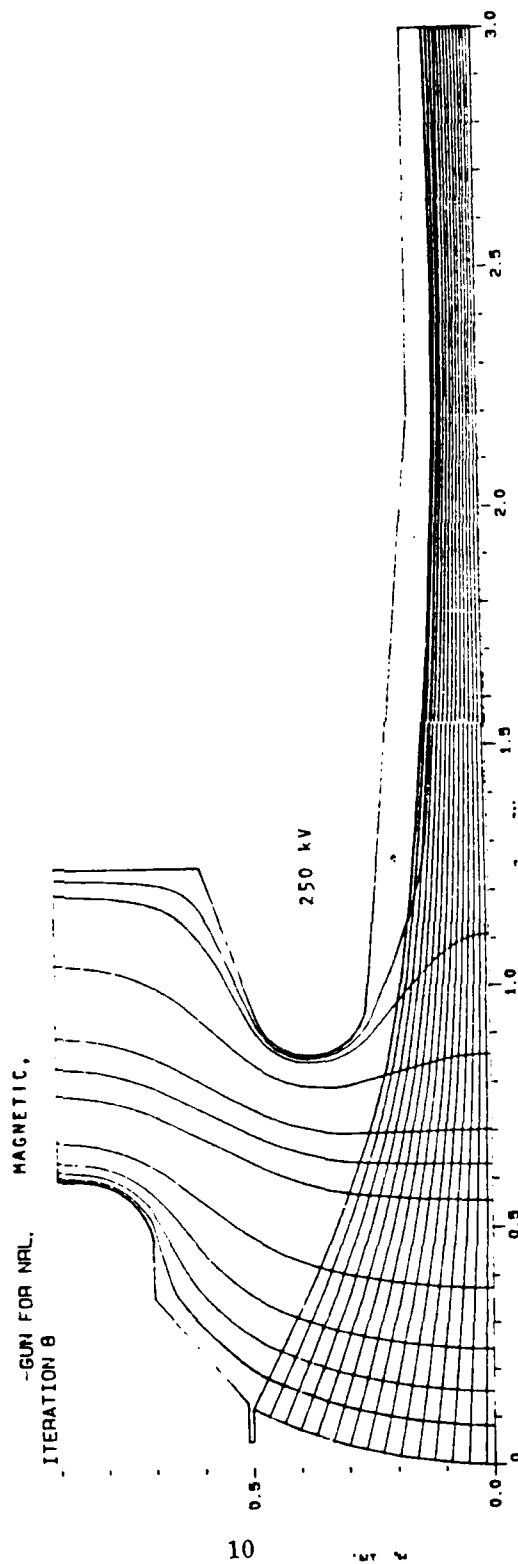


FIGURE 5. BEAM TRAJECTORIES IN CONFINED-FLOW MAGNETIC FOCUSING FIELD (250 kV)

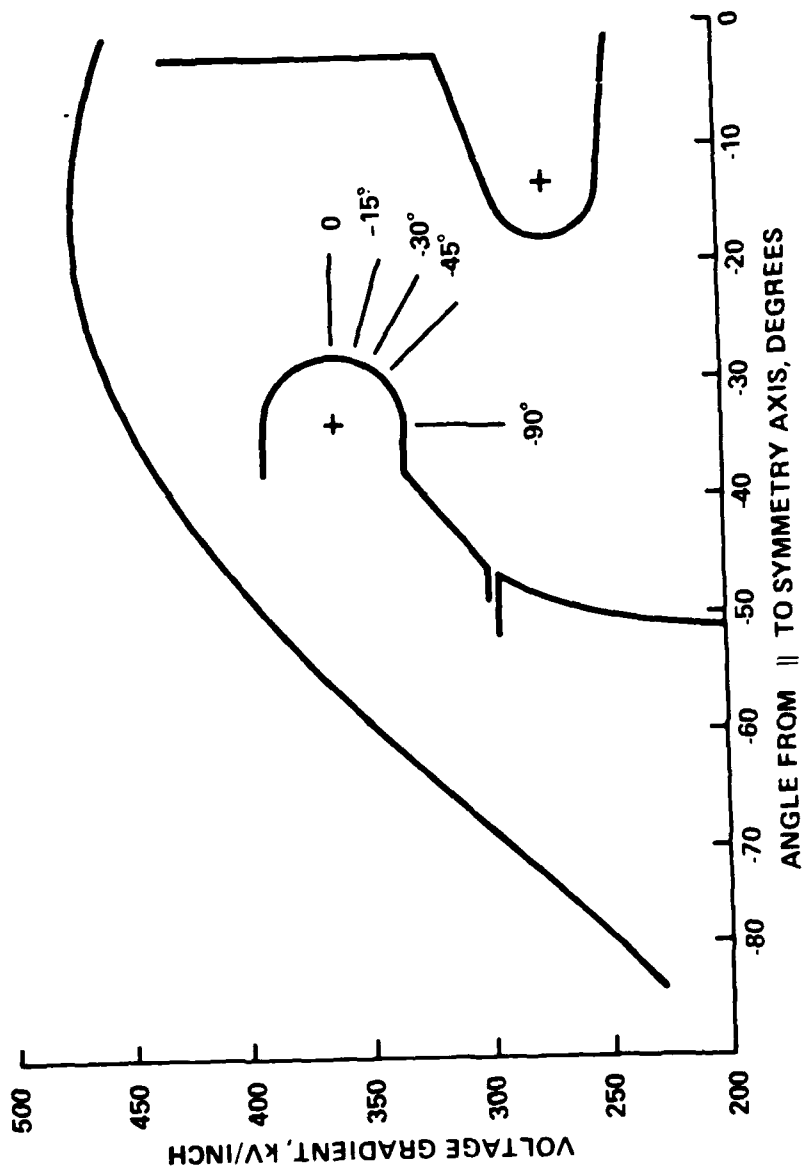


FIGURE 6. VOLTAGE GRADIENT vs FOCUS ELECTRON ANGLE

#### 4.0 ELECTRON GUN SPECIFICATIONS

The finalized electron gun specifications as per Revision A dated 13 December 1984 are summarized below:

4.1	Operating Voltage (cathode pulse)	250 kV
4.2	Cathode Current	100 Amps
4.3	Cathode Heater Voltage (Nom.) (AC)	8.5 Volts
4.4	Cathode Heater Current (Nom.)	18.5 Amps
4.5	Pulse Length (Max)	2 $\mu$ sec
4.6	Repetition Rate (Max)	100 Hz
4.7	Beam Radius (in 2.5 kG Magnetic Field)	< 0.4 cm
4.8	Beam Centroid Offset ( in 2.5 kG magnetic field)	<0.005 cm
4.9	Beam Axial Velocity Spread (biased standard deviation)	<0.4 % with a goal to 0.1% (= 8.5% beam ripple)
4.10	Beam Ripple (measured)	<20%
4.11	Concentricity of Cathode and Anode	$\pm$ 0.004 inch
4.12	Angular Deviation (tilt) of Cathode and Anode Relative to Gun Axis (Max)	0.005 radius
4.13	Lifetime (Min)	5000 hrs
4.14	Capacitance (Max)	150 pF
4.15	Gun Connection to Tube (exit drift tube dia to be determined)	2-1/8" dia. Conflat <sup>®</sup> Flange
4.16	Gun Housing Dimensions	<SLAC XK-5 dimensions



## 5.0 ASSEMBLY DRAWINGS AND MATERIAL LIST

The electron gun is constructed from three major subassemblies as illustrated in Figure 7.

- High-Voltage Seal (Drawing Items 1 and 3)
- Cathode Assembly (Drawing Item 2)
- Iron Housing and Anode Assembly (Drawing Items 5 and 6)

The high-voltage seal and vacuum housing configuration is consistent with the design utilized in the SLAC XK-5 klystron gun. Assembly and detail drawings of the gun with a parts and material list are given in Appendix A. Cathode assembly is centered in the high-voltage seal assembly within 0.001 in all directions and secured to the base. (Heliarc area at point -3.626 and its associated dimensions are used for centering.)

Iron housing and anode assembly centering also related to the same -3.626 point with its own associated dimensions.

Finally, the iron housing is heliarced to the high-voltage seal assembly.

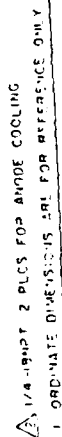


FIGURE 7. ELECTRON GUN ASSEMBLY DRAWING (K-9025)

## 6.0 TEST RESULTS

### 6.1 HIGH-VOLTAGE HOLD-OFF TESTS

High-voltage tests were conducted on gun S/N 101. A negative dc voltage was applied to the cathode and gradually raised to 150 kV dc. This level of voltage was held for 10 minutes without arcing and is considered safe for low duty 300 kV two microsecond pulses. See reference in Appendix B titled "Electron Gun Breakdown" by Armand Staprans, Varian Associates, Inc., presented at the 1985 High-Voltage Workshop, February 26, 1985, Monterey, California.

### 6.2 BEAM ANALYZER TESTS

The first electron gun was tested in the Varian computer-controlled beam analyzer at non-relativistic voltages. The beam tester configuration used in these tests is illustrated in Figure 8. An electrostatic beam profile is shown in Figure 9. The beam diameter, perveance and beam minimum position closely corresponded to the computer predictions.

Magnetic beam analyzer tests have produced an excellent beam with the required perveance and beam diameter. The confined flow beam profiles for the gun are shown in Figure 10. To analyze the quality of the beam optics and magnetic match, the magnetic field was varied from 70 to 110% of the prescribed value with no change in the beam diameter or scalloping. Scalloping was measured to be below 3% in all cases.

A gun coil was used to trim the magnetic field threading the cathode. Varying the field in the gun coil affected the beam diameter with no significant effect on the scalloping. A three-dimensional beam shape in a confined-flow focused magnetic field is illustrated in Figure 11.

### 6.3 HIGH-VOLTAGE TEST

A short drift tube and isolated collector were fabricated and attached to the gun by means of a 2-3/4 inch Varian Conflat flange. The gun-body-

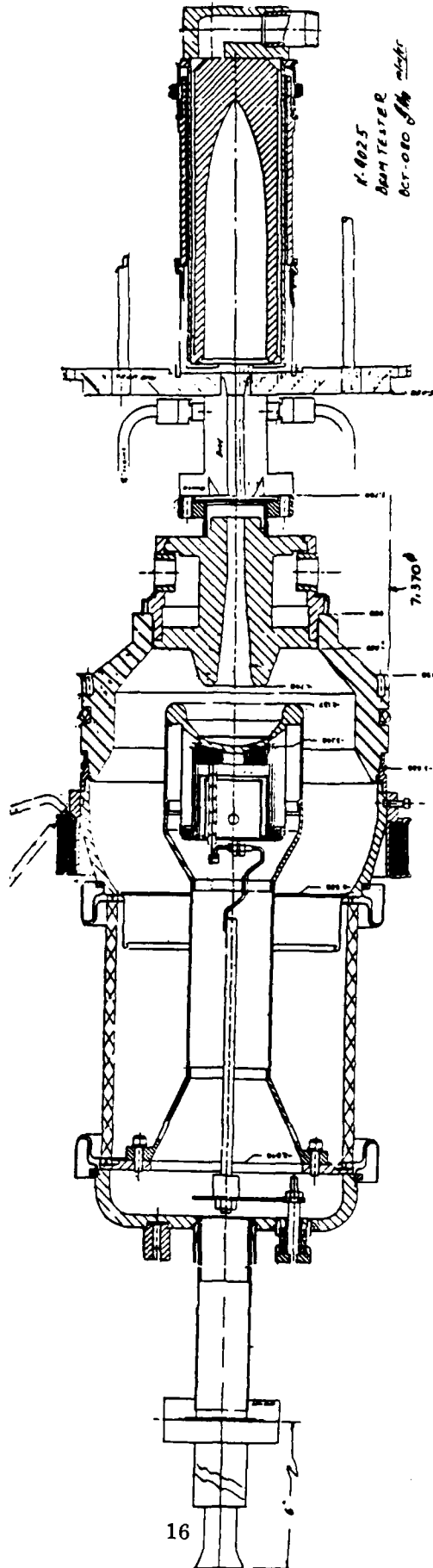


FIGURE 8. BEAM TESTER WITH K-9025 GUN



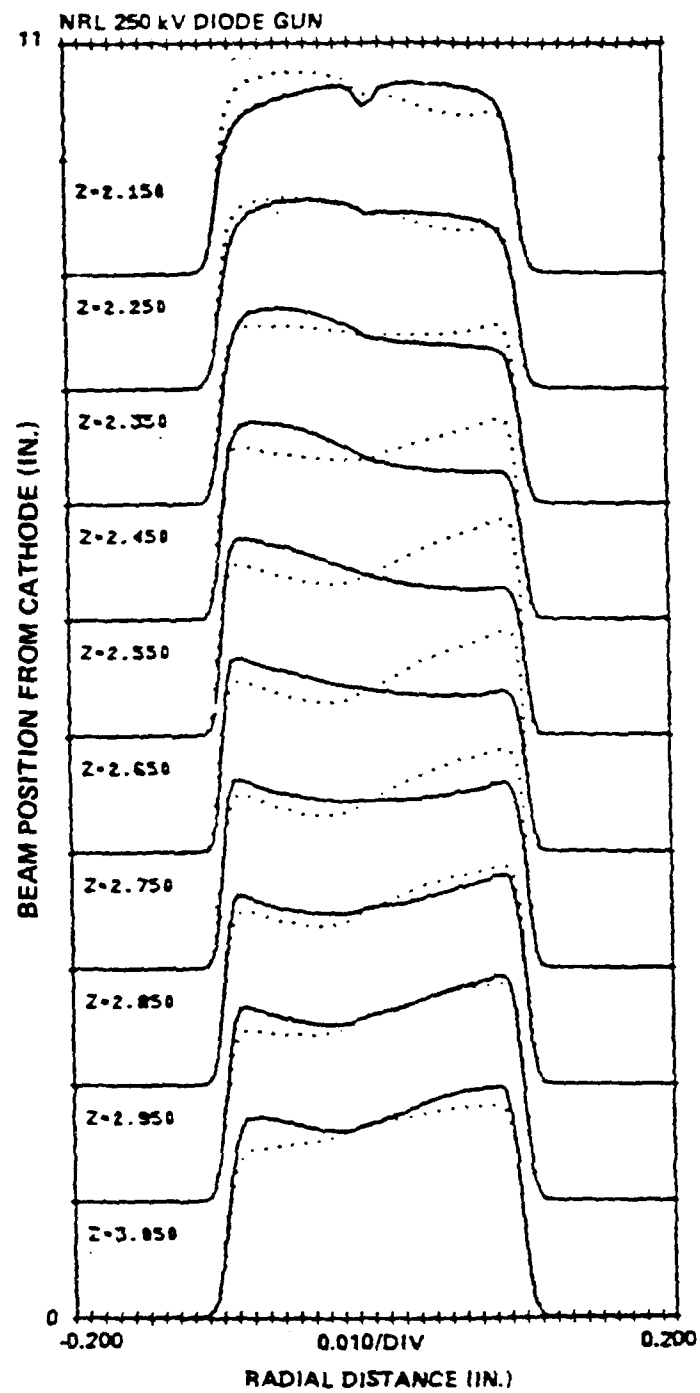


FIGURE 10. CONFINED-FLOW BEAM PROFILES

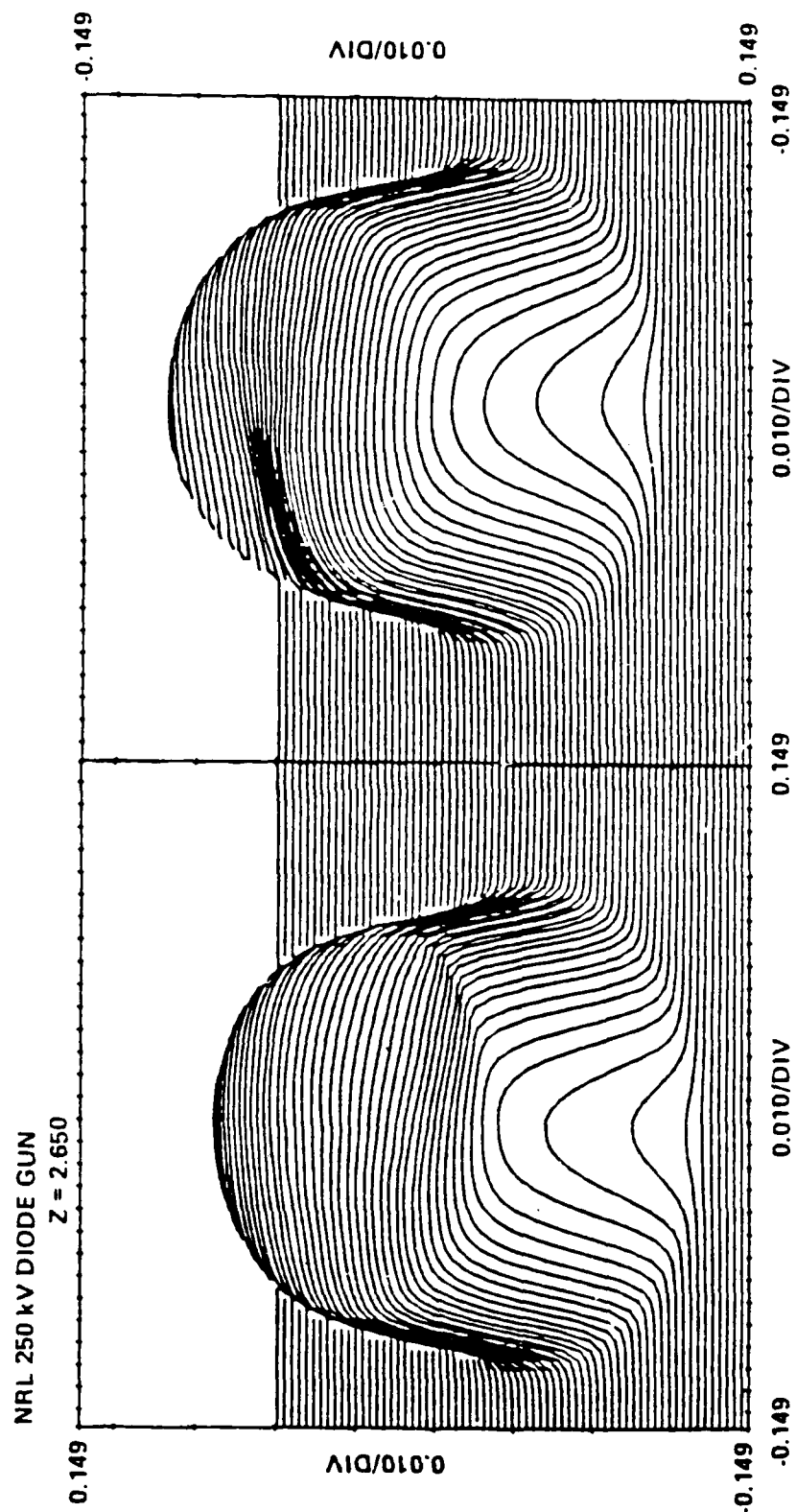


FIGURE 11. 3-D CURRENT DENSITY PROFILES

collector assembly was exhausted, baked out at 450°C, pinched off and tested under oil up to 150 kV dc.

#### 6.4 CONCLUSION

A high-quality, high-voltage gun with excellent beam laminarity has been developed for fast-wave device applications. The beam tester has been fabricated and is ready for test and evaluation. This high-power evaluation will be evaluated at NRL.



## APPENDIX A

1. ELECTRON GUN ASSEMBLY DRAWING
2. DETAIL PARTS DRAWINGS  
(Varian Associates, Inc.)
3. DETAIL PARTS DRAWINGS  
(SLAC)
4. PARTS AND MATERIALS LIST

APPENDIX A-1

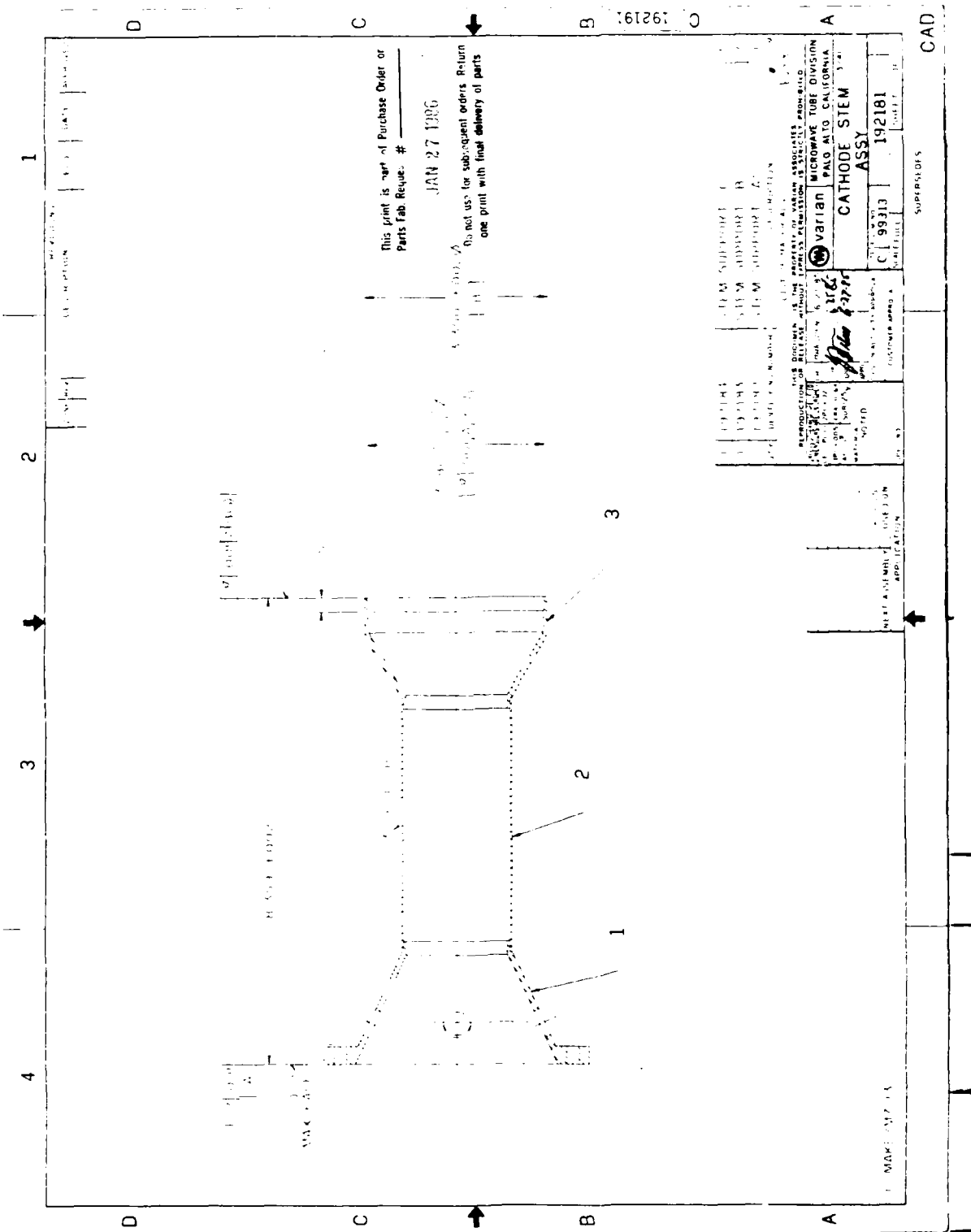
ELECTRON GUN ASSEMBLY DRAWING

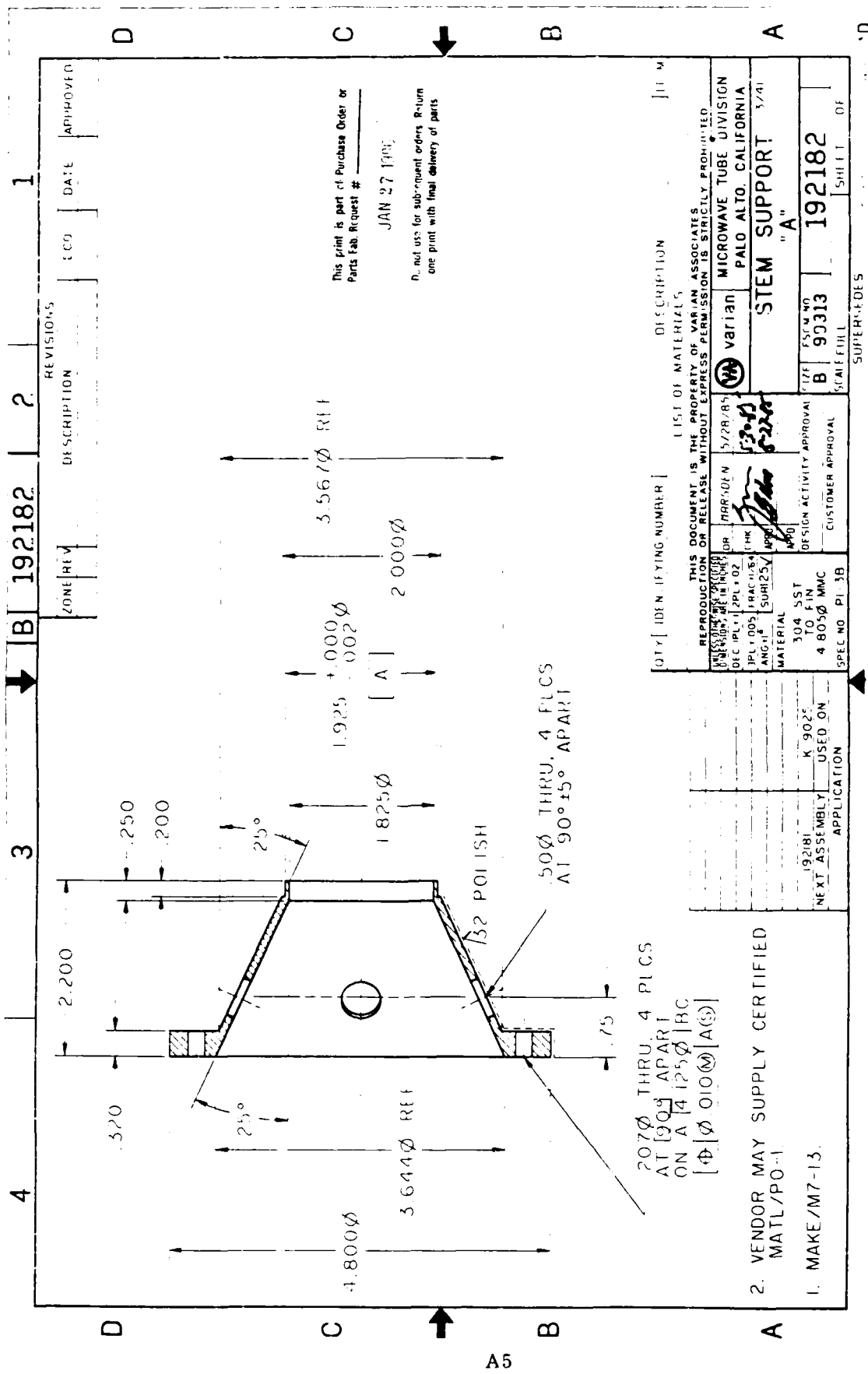


APPENDIX A-2

DETAIL PARTS DRAWINGS  
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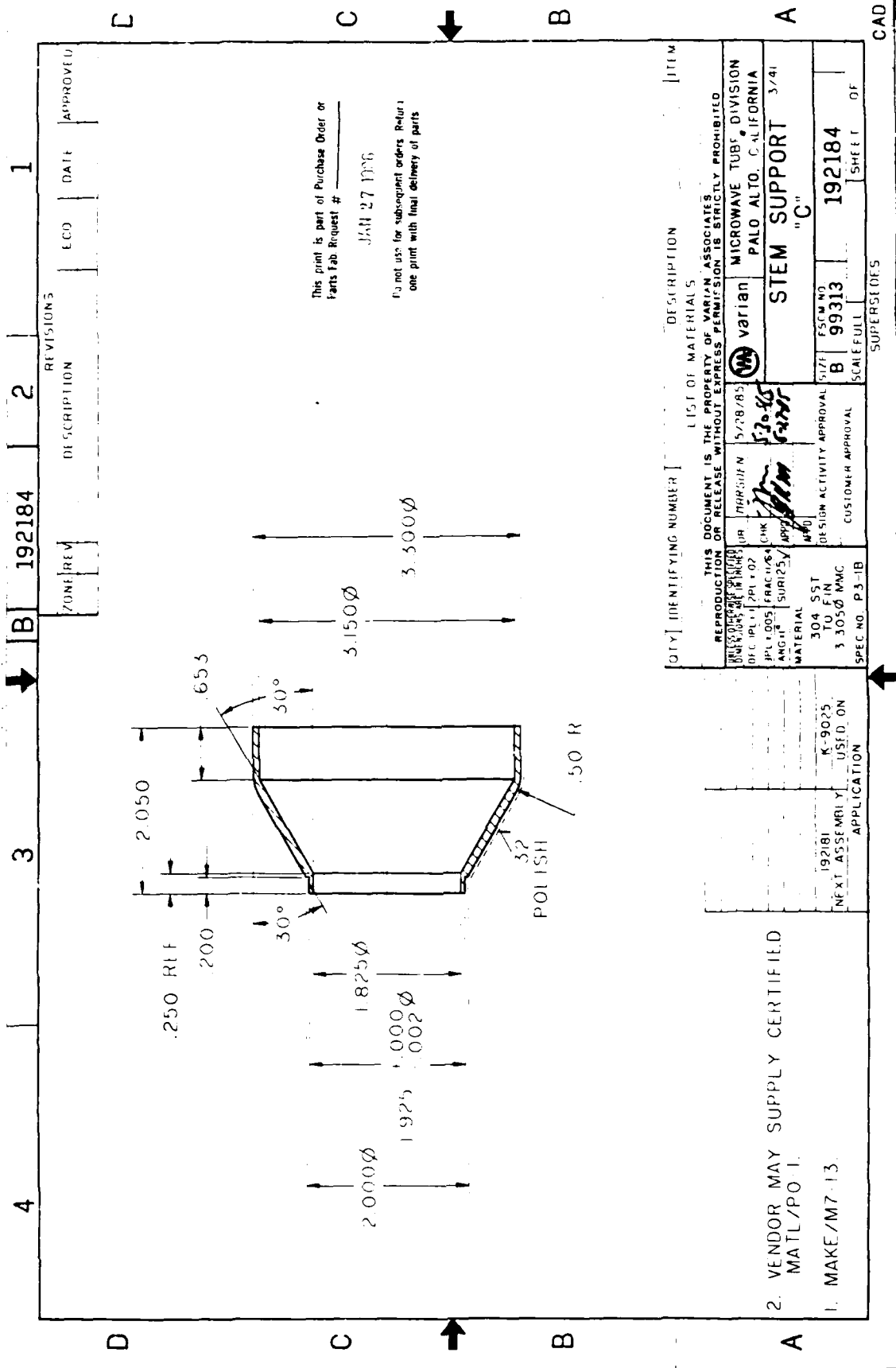
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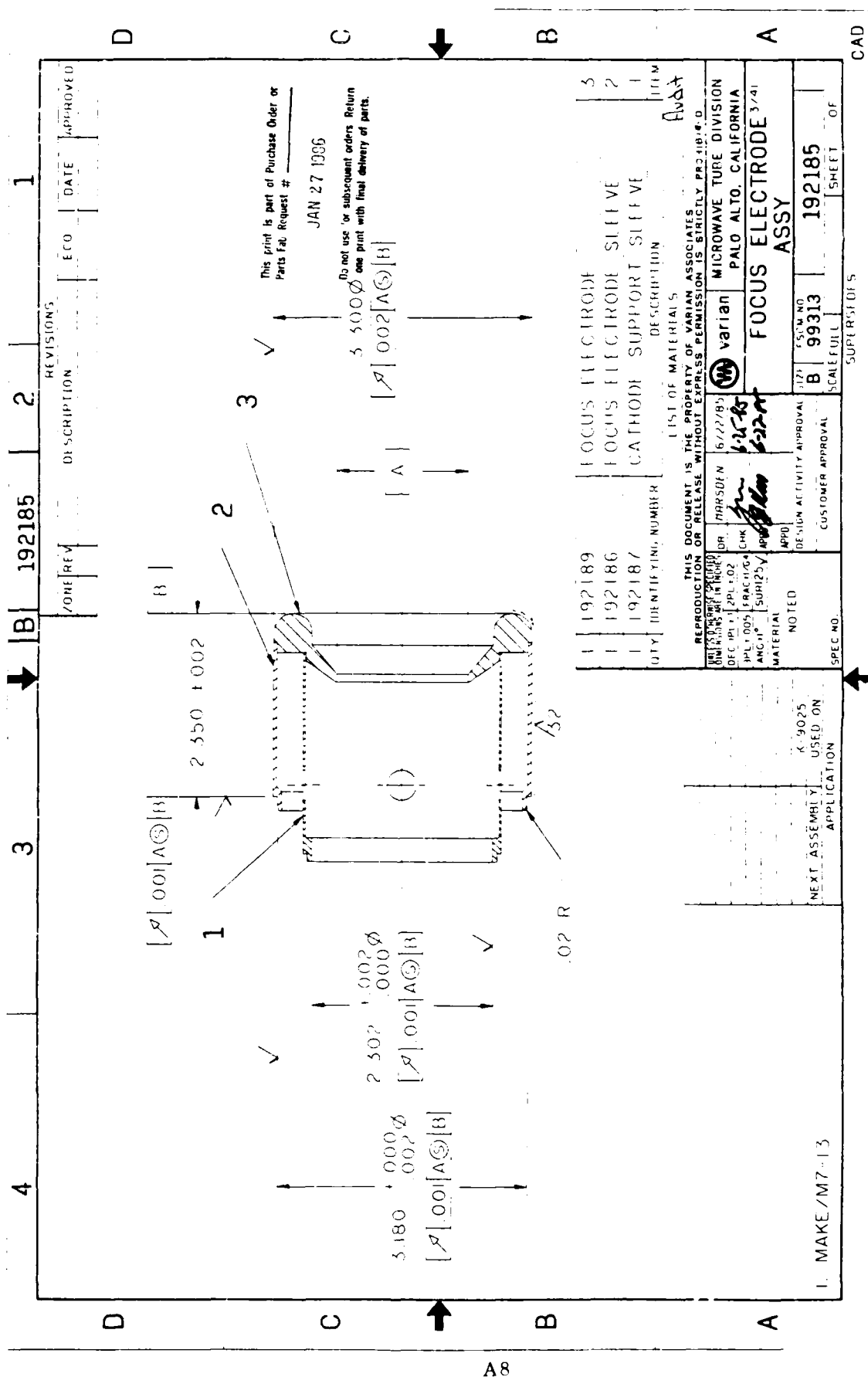
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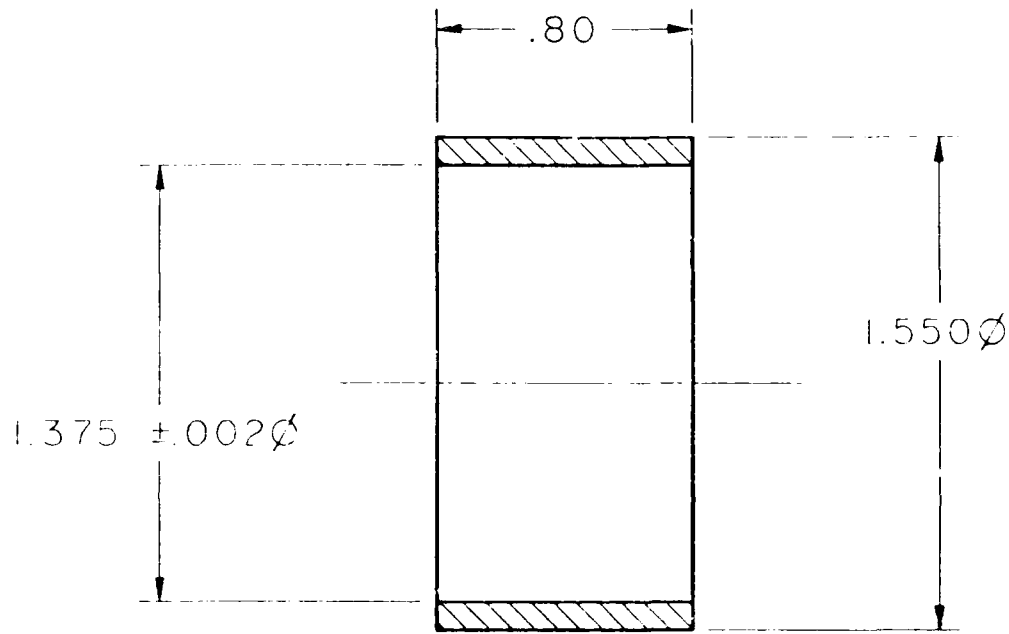






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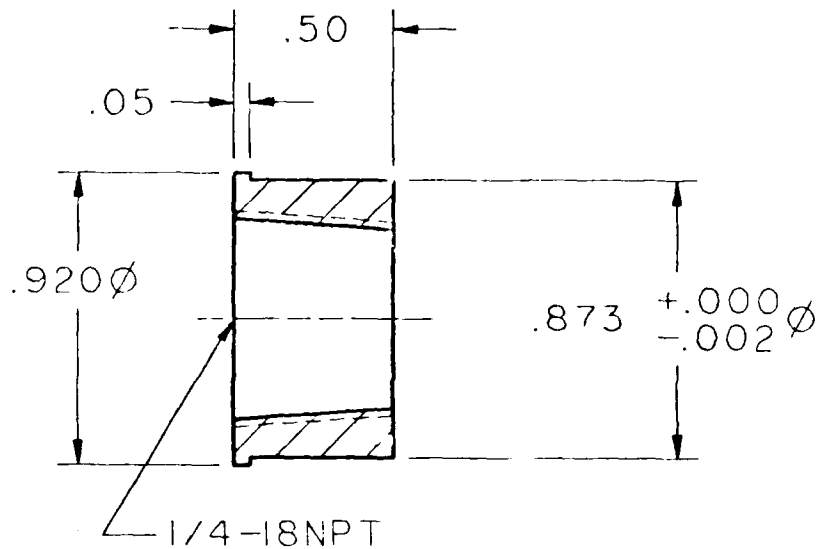
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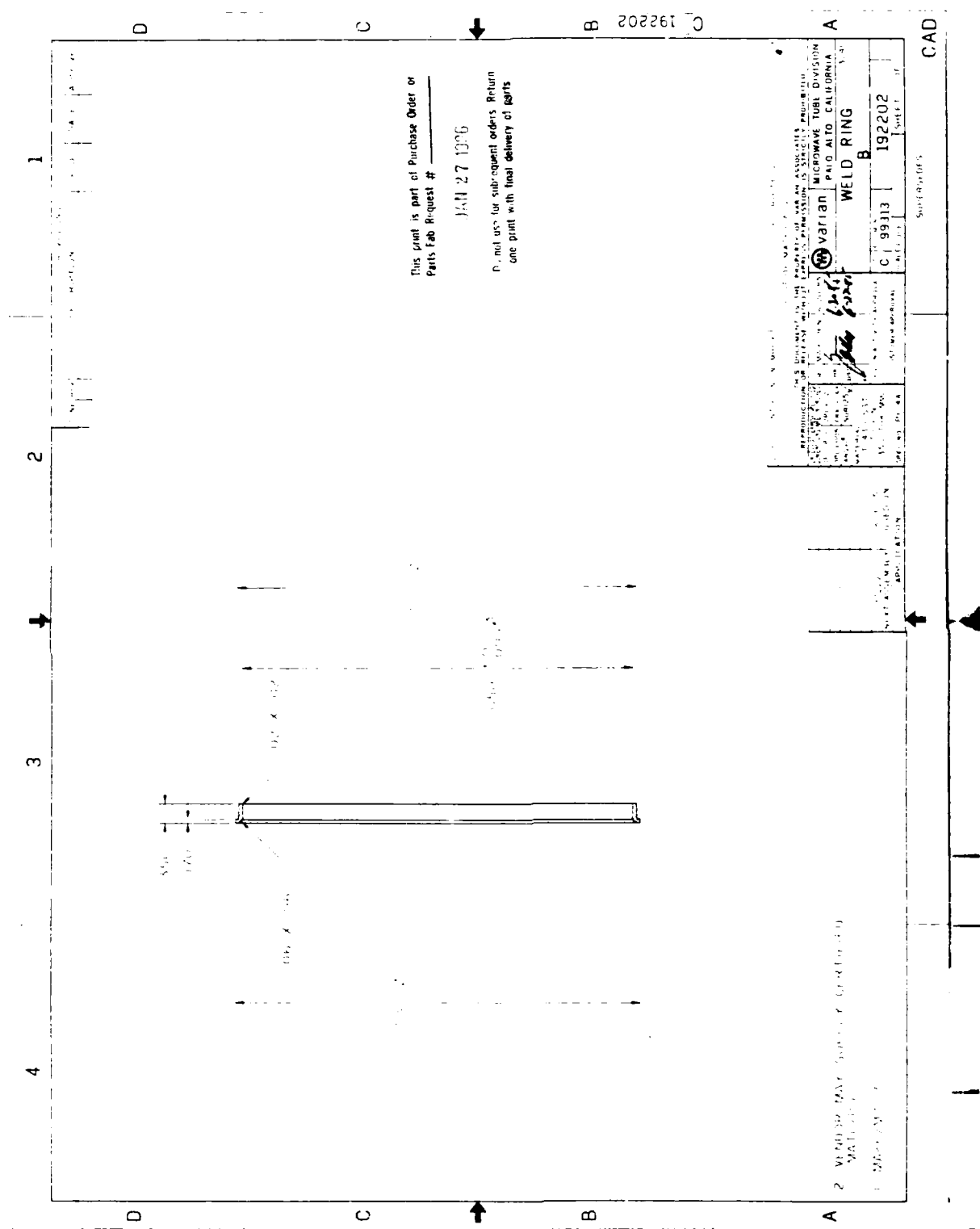
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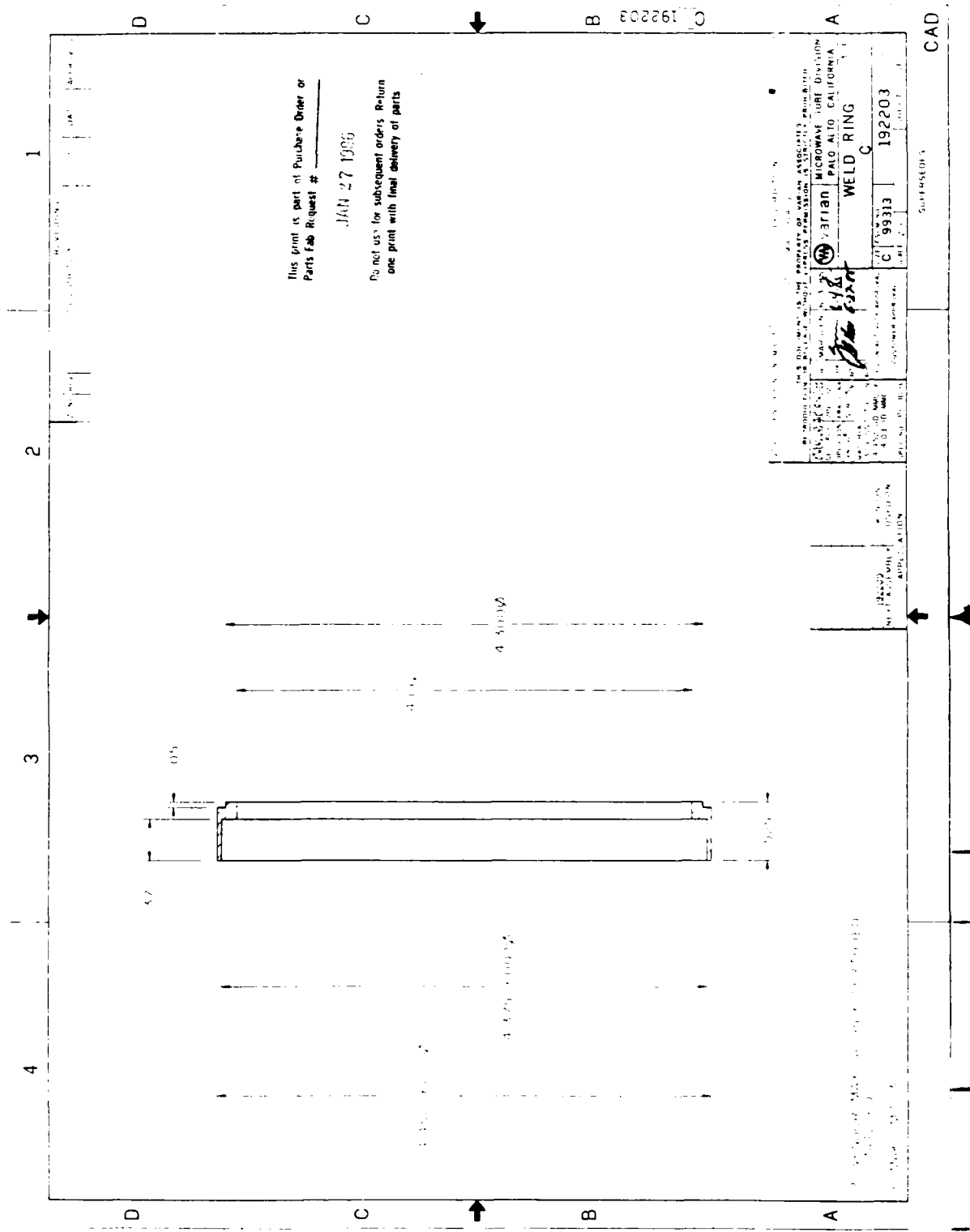
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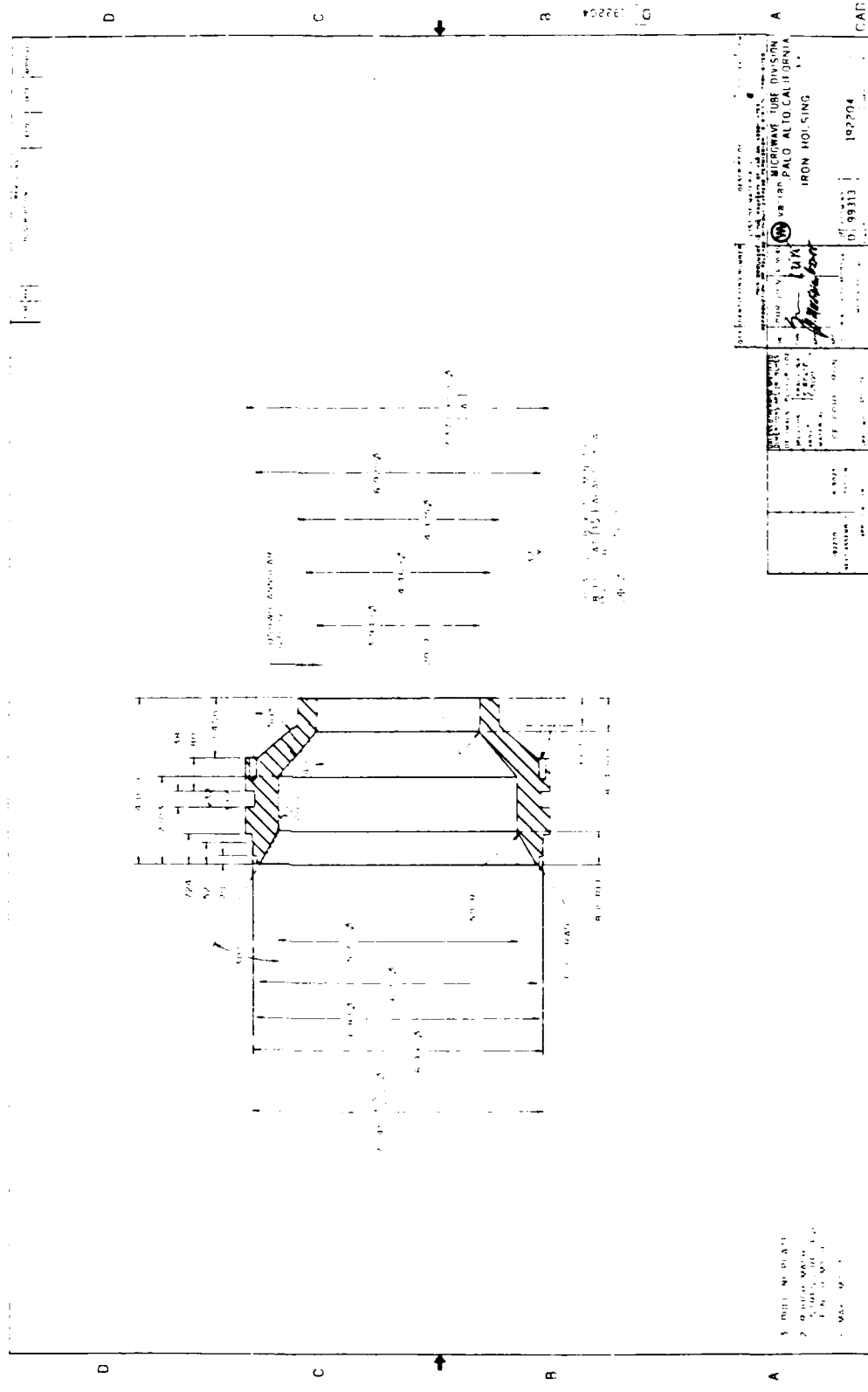
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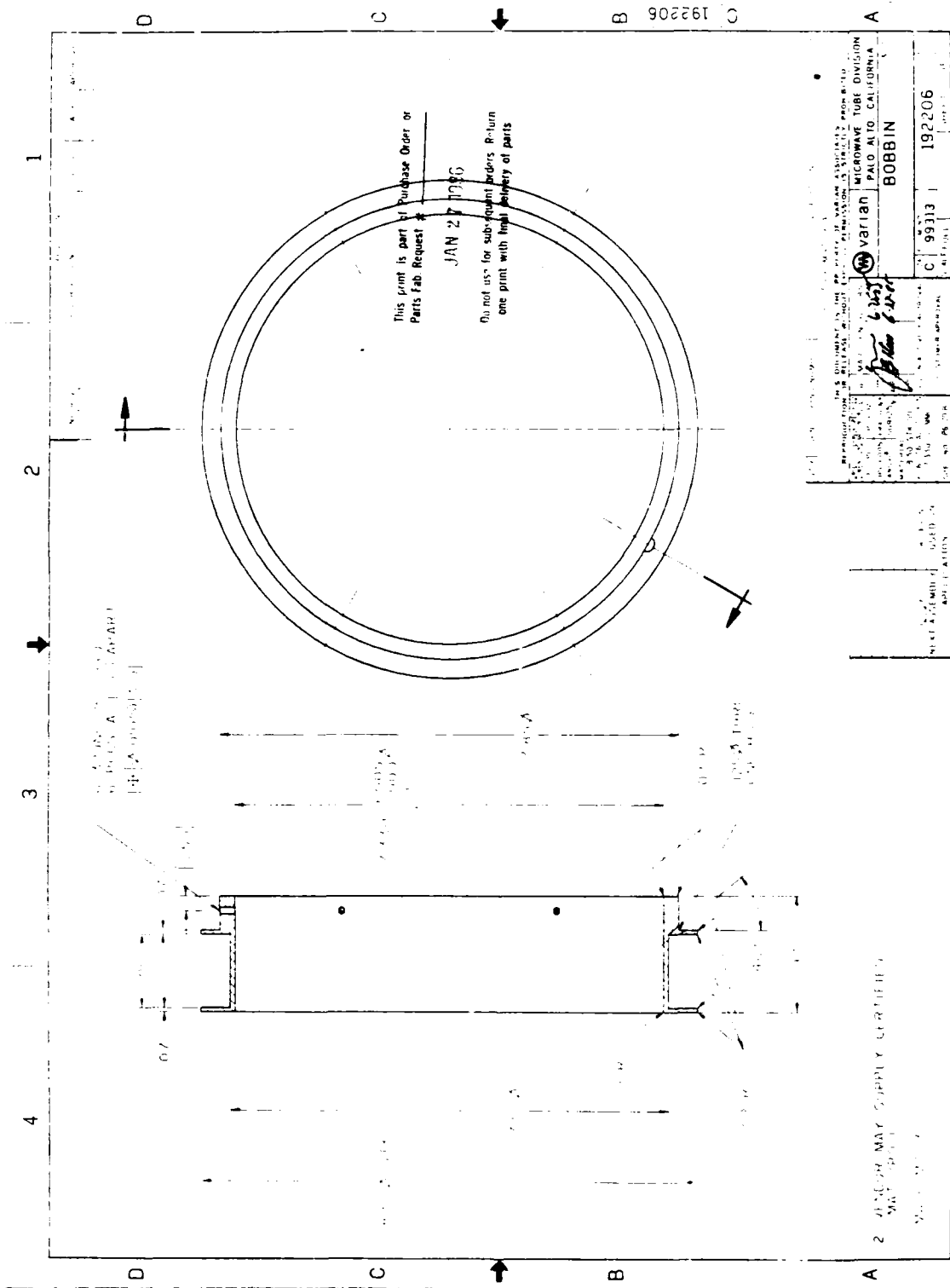
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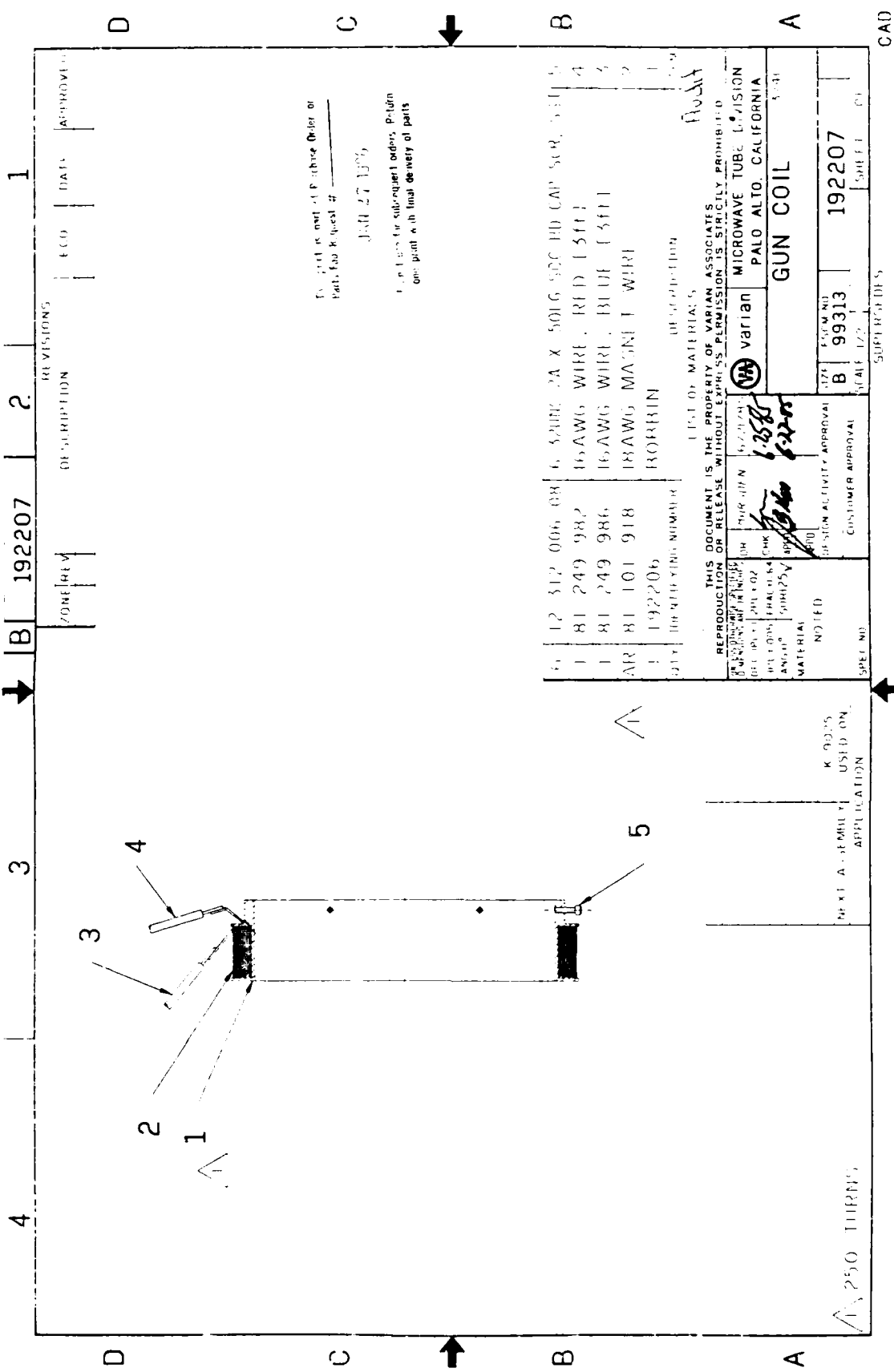




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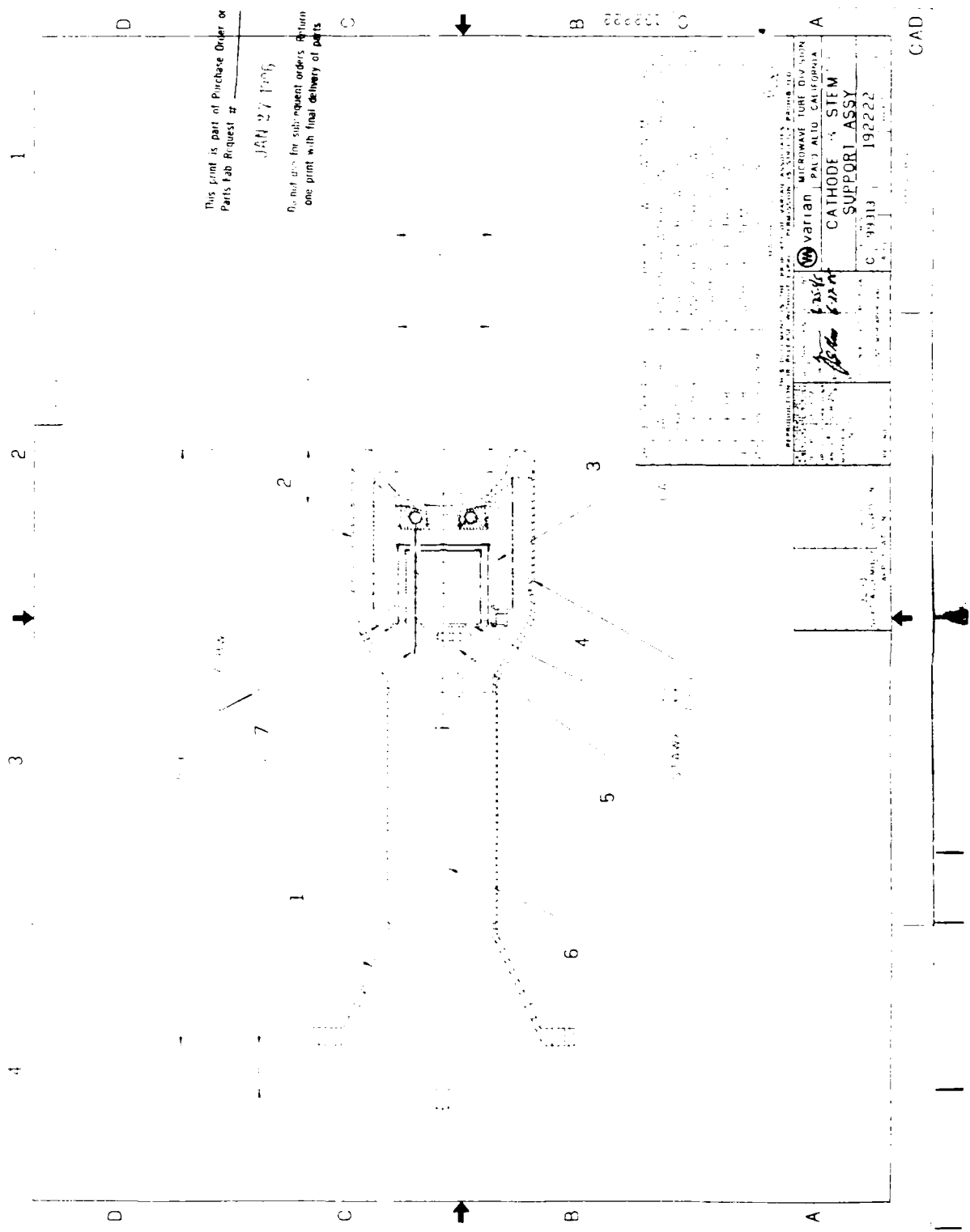


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99		192207		192207		192207	
100		192207		192207		192207	

For part or part of this Order or  
Part, for Request # \_\_\_\_\_  
Date 27 1956  
For part or part of this Order or  
Part, for Request # \_\_\_\_\_  
Date 27 1956  
For





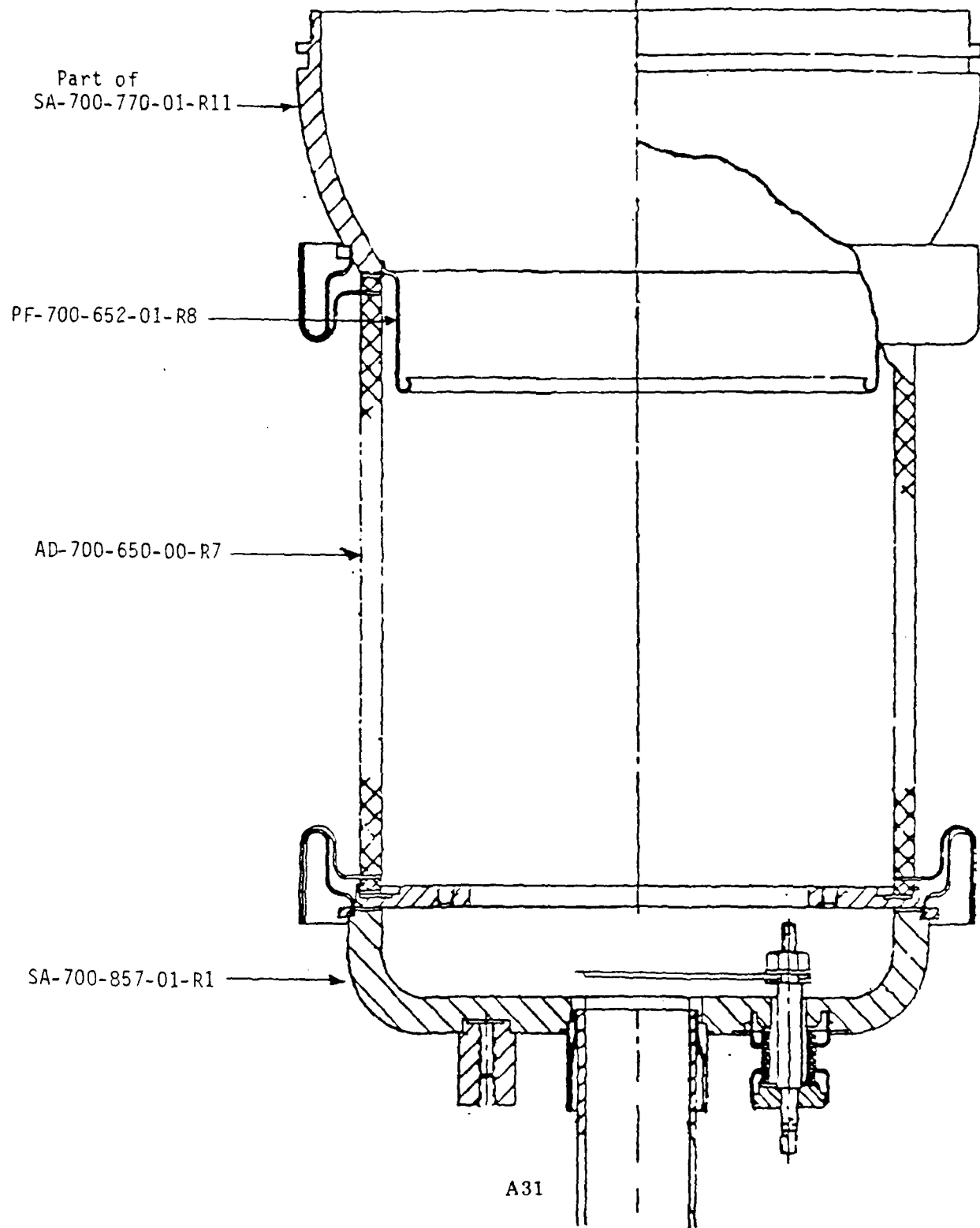


APPENDIX A-3

DETAIL PARTS DRAWINGS  
(SLAC)



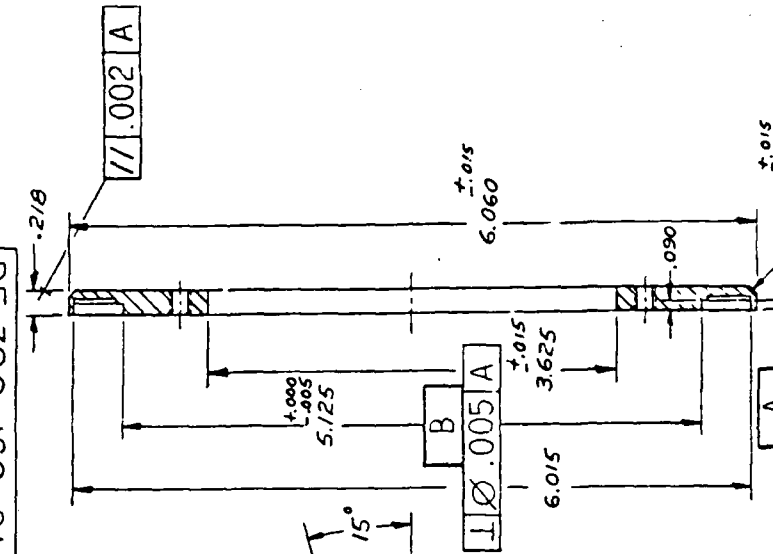
XK-5 SLAC GUN PARTS USED IN NRL GUN K-9025



XK-5 SLAC PARTS USED IN NRL GUN K-9025

<u>Title</u>	<u>Part No.</u>
Base-2 Gun Mount	PF-700-160-01-R8
Cath. Holdown Screw	212-01-R5
Ring Reinforcing	227-01-R6
Slip Ring	228-01-R7
Cylinder, Ctr. Heater	229-01-R9
Base Cup, Forming	287-01-R5
Cup, Base-finished	288-01-R15
Take-apart Joint-outer	297-01-R10
Anode Housing Blank	301-03-R10
Ring, Back Up	648-01-R5
Ceramic	649-01-R3
Assy, Seal-ceramic	AD-700-650-00-R7
Ring, Corona	PF-700-652-01-R8
Cup, Sealing-male	654-01-R7
Tube, Pumpout	655-01-R5
Housing, Anode	682-01-R15
Rod, Center Heater	759-01-R7
Assy, Anode Shell (Mach)	SA-700-770-01-R11
Asm. Ctr. Heater Cond.	783-01-R4
Assy Pumpout	857-17-R0
Ring, PL-back Up	PF-700-862-04-R0
Ceramic, Plated	862-05-R0
Assembly, Base Cup	SA-700-857-01-R1

PF-700-160-01-R8



#10-32 NF-2 THRU 4 HOLES  
EQUALLY SPACED ON  $5.125 \pm .005$  DIA B.C.

$1.005 \pm .005$  A

#10-32 NF-2 THRU 3 HOLES  
AT  $120^\circ$  APART ON  
5.570 DIA B.C.

$1.005 \pm .015$   
375 DIA X .030 DP  
4-PLCS  $90^\circ$  APART  
ON 5.640 DIA B.C.

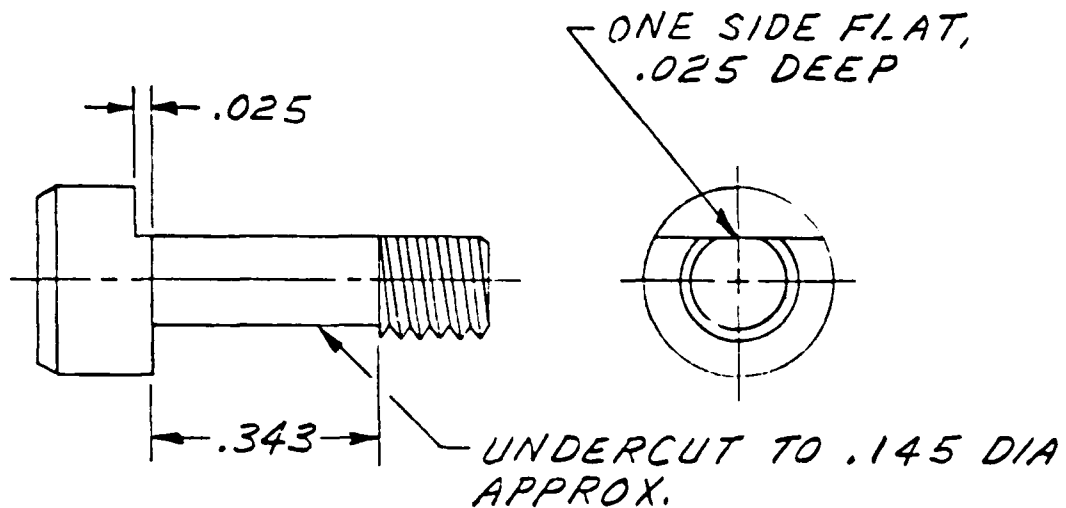
A33

- NOTE:
1. MAT'L: #304 STN STL
  2. STRESS RELIEVE AT  $950-1000^\circ\text{C}$ . FOR 10-20 MIN.  
WITH FAST COOL BEFORE FINAL MACHINING
  3. USE ONLY SLAC APPROVED MACHINING FLUIDS PER 50-700-266-47.
  4. NEXT ASSY: AD-704-011-00

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
R6	TOL. ON SIZES DIA WAS $\pm .005$	M.G.	2-6-80		1-6-83
R8	ADDED GEOM. TOLER - NOTES 3 & 4	J.G.	1-4-84	R.T.H.	1-11-84
R7	REV. NOTES	M.G.	10-20-77		10-2-82

STANFORD LINEAR ACCELERATOR—M U.S. ATOMIC ENERGY COMMISSION		TITLE BASE-2, GUN MOUNT K-5 KLYSTRON	
ENGR.	CHKD.	DATE	SCALE
DITS GREENWALD	K.L.S.	11-11-84	1:1
APPROVED		PF-700-160-01-R8	

F-1 A8



**NOTE:**

1. MADE FROM ST'D #10-32 NF-2 X 1/2 LG.  
SOC HD CAP SCR, #304 STN STL
2. USE ONLY SLAC APPROVED MACHINING FLUIDS  
PER SC-700-B66-47.
3. NEXT ASSY: AD-704-011-00

IN USE ONLY  
STANFORD UNIVERSITY  
SLAC  
ATLAS  
11-15-70

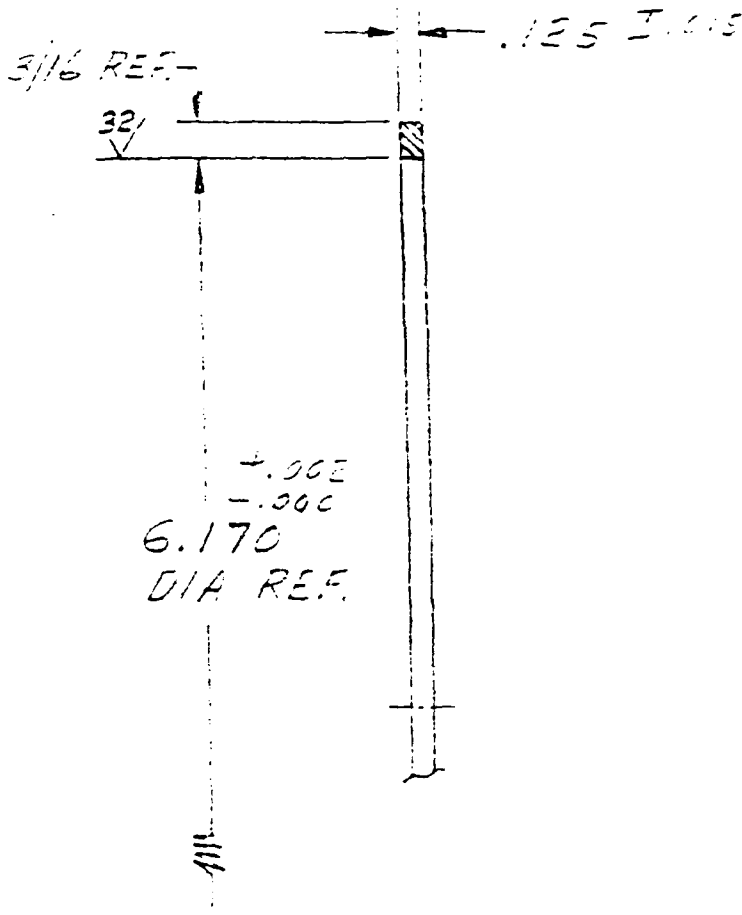
SCALE: 4" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
R3	REDRAWN & REVISED	H.G.	6-6-72	1/1/72	6-7-72
R4	CHG. TITLE	B.E.	11-15-70	ETH	11-15-70
R5	ADDED NOTE 2 & 3	J.G.	12-30-75	RTH	1/11/84

STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA		CATH HOLDOWN SCREW XK-5 KLYSTRON	
ENGR <u>R. CALLIN</u> DTS <u>H. GREENHILL</u> CNE <u>1/1/72</u>	APPROVALS <u>1/1/72</u> <u>1/1/72</u>	PF-700-212-01-R5	
		A	

1765

PROPRIETARY DATA OF STANFORD UNIVERSITY  
 RECIPIENT SHALL NOT PUBLISH THE WITHIN INFORMATION WITHOUT SPECIFIC PERMISSION  
 OF STANFORD UNIVERSITY.



NOTE:

1. MADE FROM PF-700-768-01

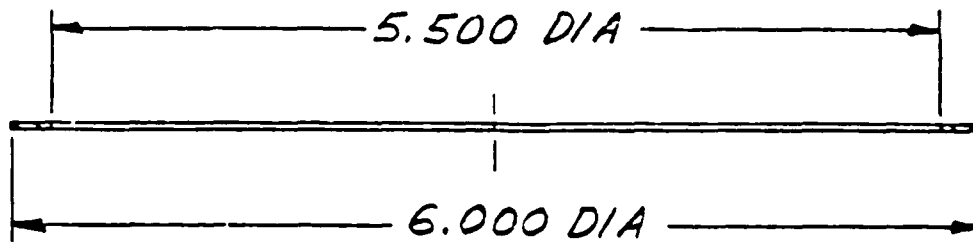
UNLESS NOTED  
 TOLERANCES BREAK CORNER .015  
 FRACT = 1/64  
 DEC. = .005  
 ANGLE = 12°  
 63

SCALE: 1" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
R2	REVISED & REDRAWN	H.G.	10-13-67	H.P.M.	10-13-67
R3	.032 X .032 BRAZE GROOVE WAS .042 X .042	H.G.	11-28-67	A.S.	11-28-67
R4	CHG. TITLE	H.G.	8-19-70	R.C.	8-19-70
R5	CHG. TITLE	H.G.	11-18-70	P.F.	11-18-70
R6	DEL. BRZ. GROOVE	S.S.	1-22-80	H.G.	1-22-80

STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA		RING, REINFORCING XK-5 KLYSTRON	
ENGR. <u>R. STRINGALL</u> DPTS. <u>H. GREENHILL</u> CHK. <u>PM</u>	APPROVALS 10-13-67	PF-700-227-01-R6	A

PROPRIETARY DATA OF STANFORD UNIVERSITY AND/OR U. S. ATOMIC ENERGY COMMISSION.  
 RECIPIENT SHALL NOT PUBLISH THE WITHIN INFORMATION WITHOUT SPECIFIC PERMISSION  
 OF STANFORD UNIVERSITY.



**NOTE:**

1. MAT'L: .005 OR .007 MOLYBDENUM
2. CHEMICAL CLEAN BEFORE PUNCHING
3. NEXT ASSY: AD-704-011-00.

LETTER NO 100  
 TOLERANCES BASIC DIMENSIONS  
 FRACTION 1/64 INT. RAD. .005  
 DEC. 2 305 63  
 ANGLE 1/2°

SCALE: 1" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
P3	REDRAWN & NOTE 2 ADDED	H.G.	12-2-69	RJC	12-2-69
R4	CHG. TITLE	H.G.	6-19-70	H.G.	6-19-70
R5	CHG. TITLE	H.G.	11-15-70	H.G.	11-15-70
R6	CHG. .007 TO .005 OR .007	S.S.	2-22-80	H.G.	2-22-80
R7	ADDED NOTE 3	J.G.	12-22-83	RTD	1/11/84
STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA		SLIP RING XK-5 KLYSTRON			
ENG. R. CALLIN DTS H. GREENHILL CHE R. C. 252	APPROVALS R. C. 12-2-69	PF-700-228-01-R7		A	

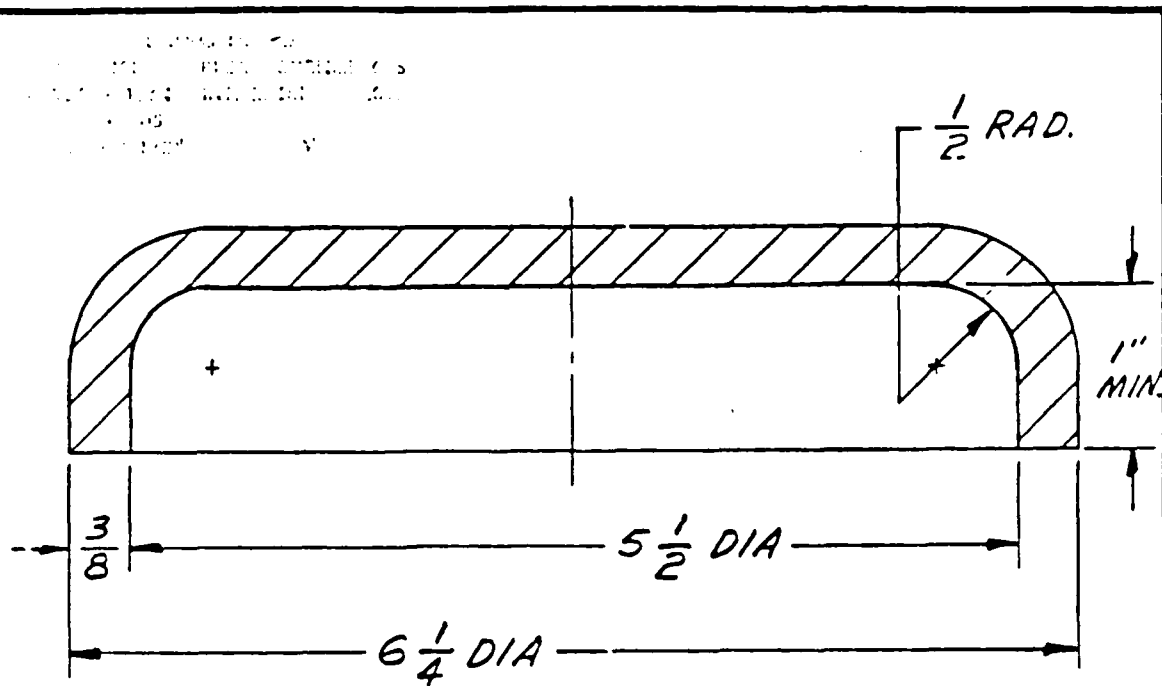
12-2-69

A36

MFF7

M/F 29

PROPRIETARY DATA OF STANFORD UNIVERSITY AND/OR U. S. ATOMIC ENERGY COMMISSION.  
RECIPIENT SHALL NOT PUBLISH THE WITHIN INFORMATION WITHOUT SPECIFIC PERMISSION  
OF STANFORD UNIVERSITY.



**NOTE:**

1. SEE PF-700-288 FOR MACHINING INFORMATION
2. BLANK SIZE =  $7 \frac{7}{8}$  RD., SAW CUT & MACHINE TO  $7.750 \pm .000$   
 $\pm .015$
3. ANNEAL AT  $750 - 800^{\circ}C$ . FOR 15 MIN.  
BEFORE FORMING

SCALE: 1"=1" MAT'L: 3/8 THK. CERT OFHC CU. PLATE

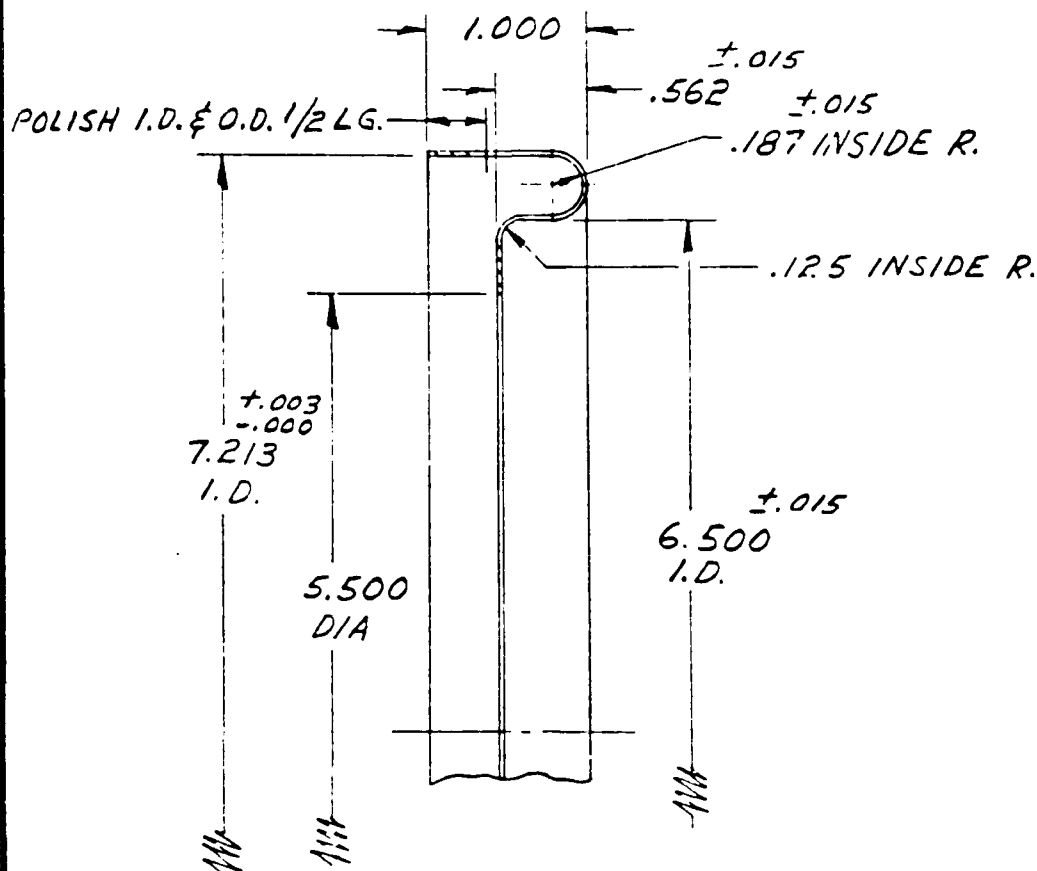
REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
R2	REDRAWN & NOTES 2 & 3 ADDED	H.G.	7-17-69	H.G.	7-17-69
R3	CHG. TITLE	H.G.	3-18-70	H.G.	3-18-70
R4	CHG. TITLE	H.G.	11-15-76	H.G.	11-15-76
R5	REV. NOTE: 3.	H.G.	10-21-85	H.G.	10-21-85

STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA		BASE CUP, FORMING XK-5 KLYSTRON	
ENGR. <u>R. COLLIN</u> DTS <u>H. GREENHILL</u> CHE <u>/</u>	APPROVALS <u>[Signature]</u> 7-17-69	PF-700-287-01-R5	A





STANFORD LINEAR ACCELERATOR  
 REVISIONS  
 1. 10-10-62  
 2. 11-23-62  
 3. 12-14-62  
 4. 1-10-63  
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 100. 1-10-63



# NOTES:

1. BLANK SIZE = 10 1/8" ROUND BLANK.
2. USE ONLY SLAC APPROVED MACH. FLUIDS PER SC-700-866-47
3. NEXT ASSY: AD-700-650-00.

UNLESS NOTED  
 TOLERANCES: DECIMAL DIMENSIONS .015  
 FRACTIONS: 1/16, 1/8, 1/4, 1/2, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100

R7	ADDED POLISH NOTE	9-13-62	1
RC	CHG TITLE	11-23-62	1
R5	CHG. TITLE	3-18-70 H.G.	1
R4	BLANK SIZE WAS 12" SQ.	12-14-62 H.G.	1
R13	ADDED NOTE 2. & 3	12-14-62 H.G.	1
PS	DEL. NOTE 2.	12-9-62 H.G.	1
RE	ADDED NOTE 2.	9-12-79 H.G.	1

STANFORD LINEAR ACCELERATOR—M  
 U.S. ATOMIC ENERGY COMMISSION

MAT'L. USED THK. 70-30 EQUIP. NO.

ENGR.                      CHK'D                       
 DFTS                      APP'D                     

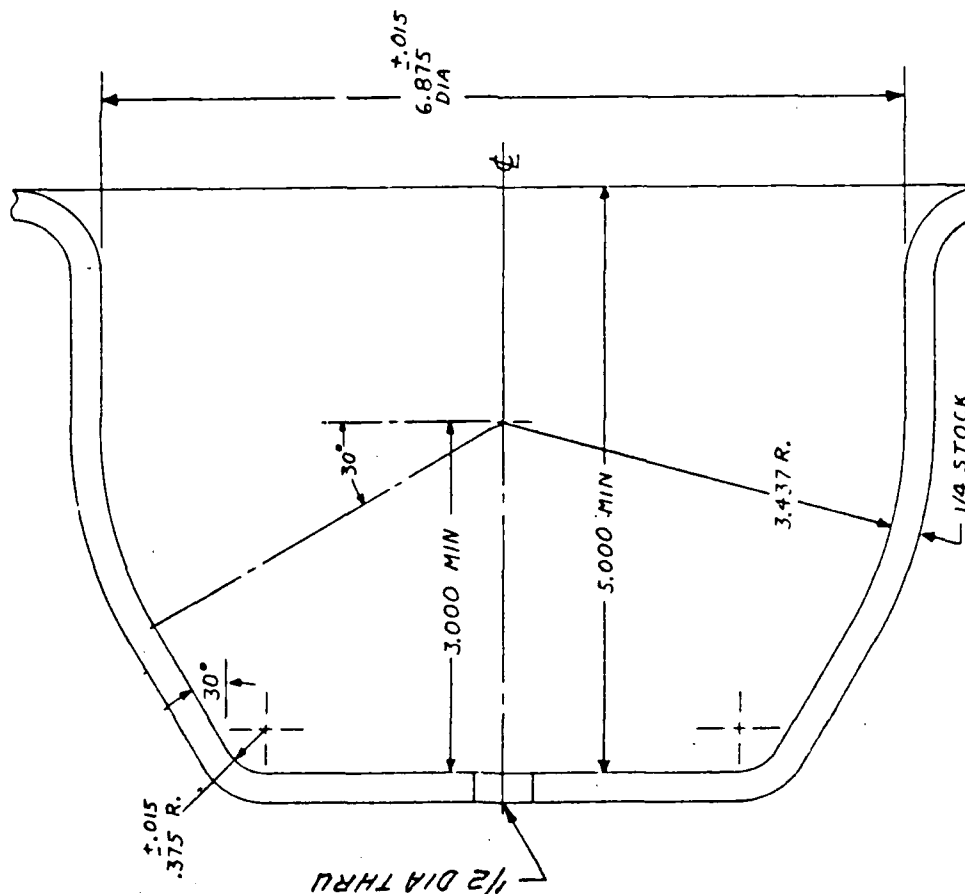
TITLE TAKE-APART JOINT-OUTER  
 XK-5 KLYSTRON

DATE 12-10-62  
 SCALE 1"=1"

PF-700-297-01-R10

PF-700-301-01-R10 B

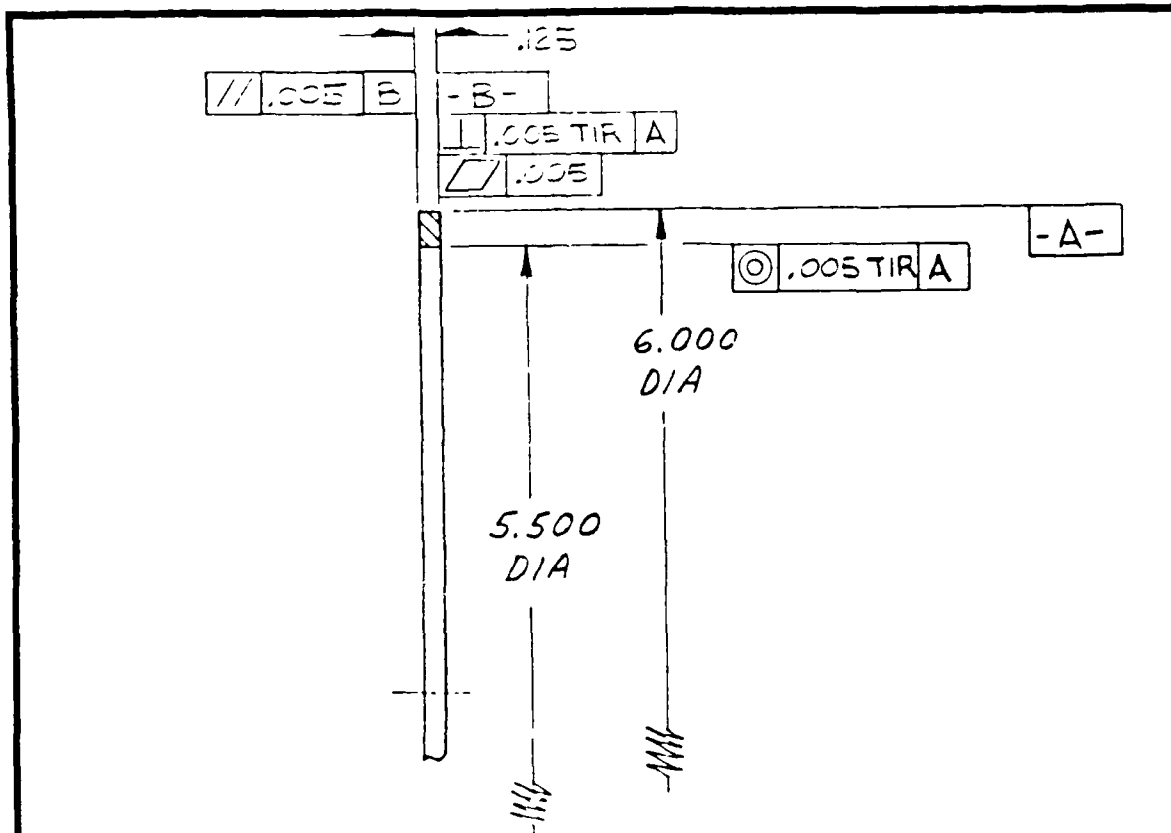
REV	DESCRIPTION	DRN	DATE	APP	DATE
R10	WAS MP-700-301-01, ADDED SPECS	H.G.	12-1-78	J.E.	12-1-78



NOTE:  
 1. MAT'L: #304 STN STL, BLANK SIZE = 16" SQ.  
 2. STRESS RELIEVE AT 950° - 1000°C. FOR 10-20 MIN., WITH FAST COOL

SCALE: 1" = 1"	DO NOT SCALE DRAWING	NEXT ASSEMBLY:
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES BEAR EDGES .005 MIN FRACT = 1/64 INT COE AND 8 MAX DEC = .005 ALL SURF V	STANFORD LINEAR ACCELERATOR CENTER U S ENERGY RESEARCH AND DEVELOPMENT ADMINISTRATION STANFORD UNIVERSITY STANFORD, CALIFORNIA APPROVALS PAGE 1 G. KONRAD DATE 12-1-78 BY H.G.	ANODE HOUSING BLANK XK-5 KLYSTRON PF-700-301-03-R10 B

PROPERTY DATA OF STANFORD UNIVERSITY  
 REPRODUCED FROM THE RECORDS OF THE  
 STANFORD UNIVERSITY



NOTES:

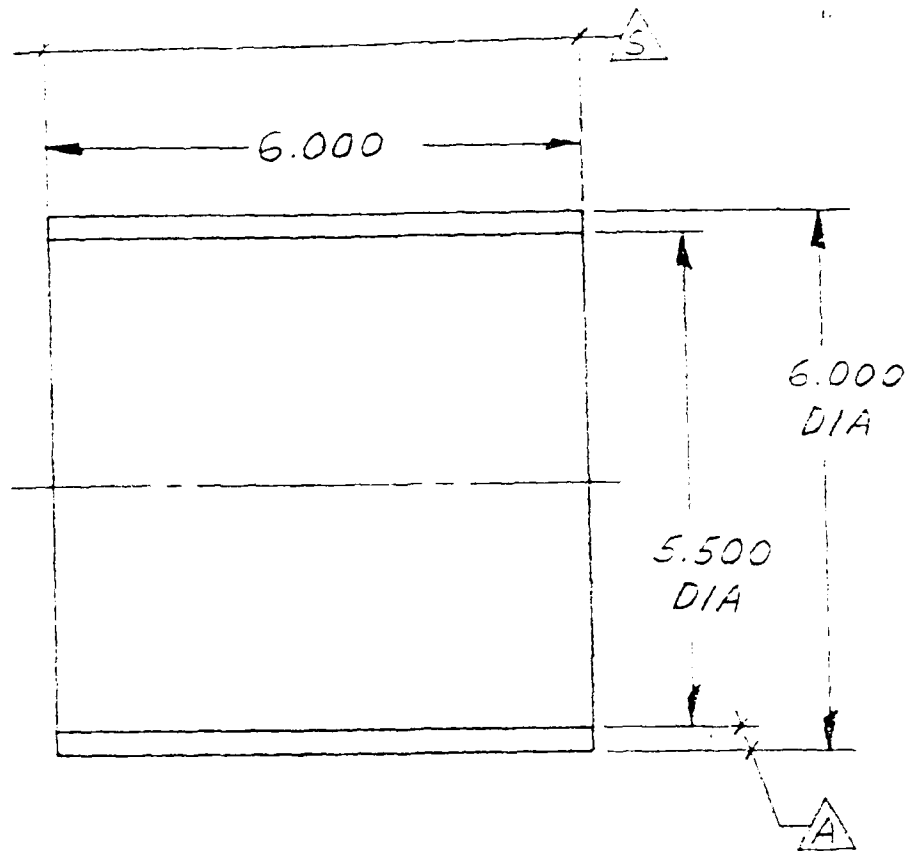
1. MADE FOR PF-700-362-04

UNLESS OTHERWISE SPECIFIED  
 DIMENSIONS ARE IN INCHES.  
 TOLERANCES: BREAK EDGES .005-  
 FRACT  $\pm .005$  INT COR .005 R MAX  
 DEC.  $\pm .005$   
 ANGLES  $\pm .5^\circ$  ALL SURFS.  $\checkmark$

RE	ADD GEOM. TOL.	5-2-63 HJ	2-2-64 RTH
R4	CHG TITLE	11-21-74 B.S.	11-21-74 HJ
R3	CHG. TITLE	8-18-74 H.G.	8-18-74 R.C.
R2	CHANGED TITLE	5-6-65 H.G.	5-6-65 R.E.B.
R1	TITLE WAS: RING, SLIP	11-14-63 H.G.	11-14-63 HJ

STANFORD LINEAR ACCELERATOR—M U.S. ATOMIC ENERGY COMMISSION		TITLE RING, BACK UP VK-5 KLYSTRON	
MAT'L. CERAMIC - AL-300			
ENGR. J.E. GREENHILL	CHK'D. H.J.	DATE 2-6-63	PF-700-648-01-RE
DFTS. GREENHILL	APP'D. H.J.	SCALE 1"=1"	

PROPERTY DATA OF STANFORD UNIVERSITY AND OF U.S. ATOMIC ENERGY COMMISSION  
 REFERENCE: STANFORD UNIVERSITY REPORT PF-700-649-01-1  
 OF STANFORD UNIVERSITY



**NOTE**

1. TWO DIA'S. **A** TO BE CONC. WITHIN .005 T.I.R.
2. TWO SURFACES **S** TO BE FLAT, PARALLEL TO EACH OTHER & PERPENDICULAR TO **A** WITHIN .005 T.I.R.

UNLESS OTHERWISE SPECIFIED  
 DIMENSIONS ARE IN INCHES.  
 TOLERANCES: BREAK EDGES .005-.015  
 FRACT.  $\pm 1/64$  INT. COR. .015 R. MAX  
 DEC.  $\pm .005$   
 ANGLES  $\pm 1/2^\circ$  ALL SURFS.

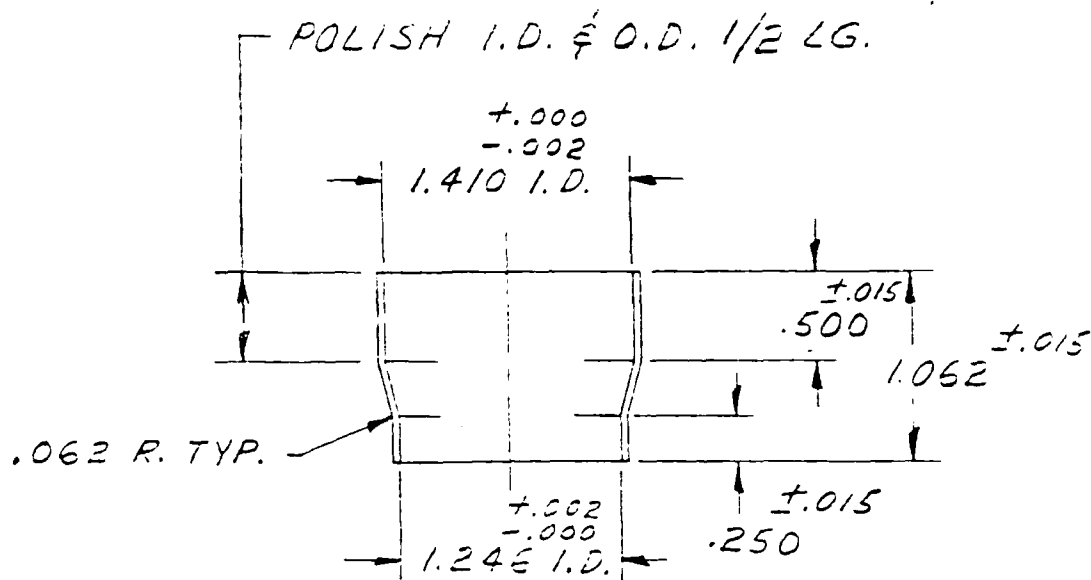
R3	CHG TITLE	11-25-76	R.E.B.
R2	CHG. TITLE	8-18-70	R.E.B.
R1	CHANGED TITLE	5-6-65	R.E.B.

STANFORD LINEAR ACCELERATOR—M U.S. ATOMIC ENERGY COMMISSION		TITLE CERAMIC XK-5 KLYSTRON	
MAT'L. CERAMIC - AL-300		DATE 2-6-63	
ENGR. MERWINIAN CHK'D H.G.		SCALE 1/2" = 1"	
DFTS. GREENHILL 2-6-63 APPY'D G.H.S.		PF-700-649-01-R3	

ITEM NO	PREFIX	BASE	SUFFIX	TITLE OR DESCRIPTION	QTY
3	BF	700-262	05	CERAMIC, PLATED	1
2	BF	700-297	01	TAKE-APART JOINT, OUTER	2
1	BF	700-242	04	FL-BACK LP	2



PROPERTY DATA OF STANFORD LINEAR ACCELERATOR—M  
 U.S. ATOMIC ENERGY COMMISSION  
 DRAWING NO. PF-700-654-01-R7



**NOTE:**

1. MAT'L: .020 THK. 70-30 CUPRO-NICKEL
2. BLANK SIZE = 3.010 DIA
3. CHEMICAL CLEAN
4. ANNEAL AT 800-850° C. FOR 20 MIN.  
BEFORE DRAWING
5. CHEMICAL CLEAN
6. STRESS RELIEVE AT 800°-850° C. FOR 20 MIN.  
BEFORE MACHINING

13 SEP 1978

UNLESS NOTED  
 TOLERANCES BREAK CORNER .005  
 FRACT. ± 1/64 INT. RADII .015  
 DEC. .005 63  
 ANGLES = 1/2°

R5	REV. NOTES	7-16-71 H.G.	123
R4	DEL. NOTES 5. & 6. CHANGED TITLE	1-23-70 H.G.	124
R3	REVISED NOTES	7-17-69 H.G.	125
R7	ADDED POLISH NOTE	9-13-78 H.G.	126
R5	CHANGED TITLE	7-17-69 H.G.	127

STANFORD LINEAR ACCELERATOR—M  
 U.S. ATOMIC ENERGY COMMISSION

TITLE CUP, SEALING-MALE  
 XK-5 KLYSTRON

ENGR. MERDINIAN CHK'D H.G.  
 DFTS GREENHILL 3-12-63 APPV'D [Signature]

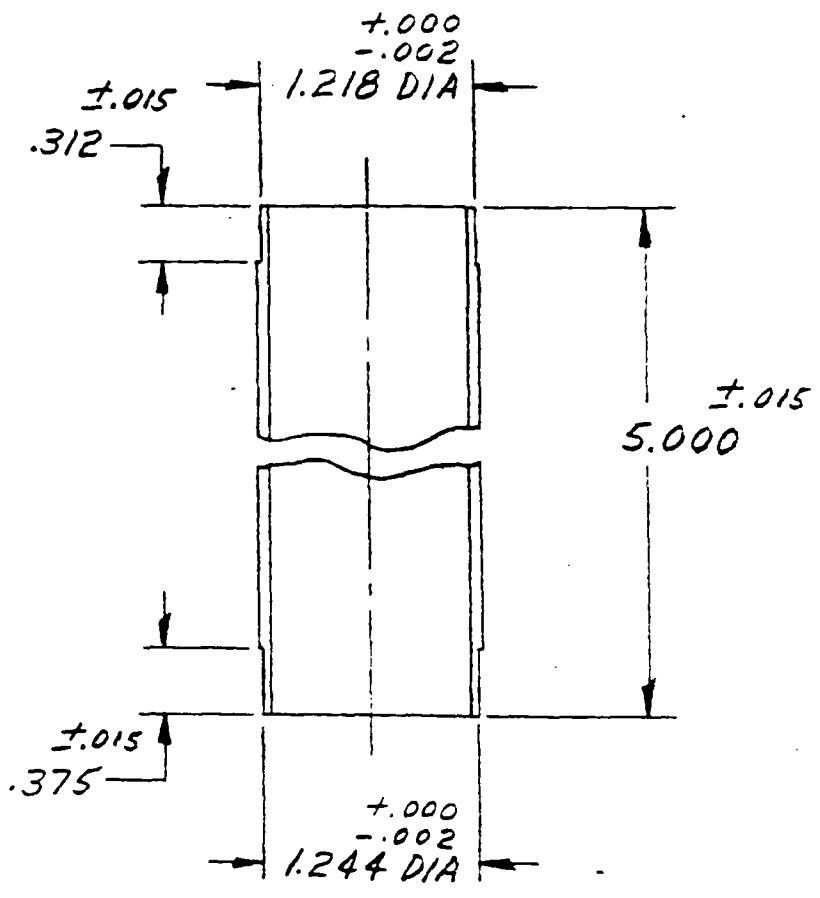
DATE 3-12-63  
 SCALE 1"=1"

PF-700-654-01-R7

PF-700-654



THIS DRAWING CONTAINS INFORMATION UNLESS SPECIFIC PROVISION  
 BE MADE TO THE CONTRARY. IT IS THE PROPERTY OF THE U.S. GOVERNMENT  
 AND IS LOANED TO YOU. IT AND ITS CONTENTS ARE NOT TO BE  
 REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS  
 ELECTRONIC OR MECHANICAL, INCLUDING PHOTOCOPYING, RECORDING,  
 OR BY ANY INFORMATION STORAGE AND RETRIEVAL SYSTEM, WITHOUT  
 PERMISSION IN WRITING FROM THE U.S. GOVERNMENT.



NOTE:  
 1. MACHINED SURFACES  $\sqrt{32}$   
 2. POLISH STOCK O.D

UNLESS NOTED  
 TOLERANCES BREAK CORNER .005  
 PRACT = 1/64 INT. RADII .015  
 DEC. = .005  
 ANGLES = 1/2° 63  
 V

5	ADDED NOTE #2.	3-8-60	R.E.B.
4	DEL. BRZ. GROOVES	3-21-80 H.G. 5.5. 3-21-80	
R3	CHG. TITLE	11-23-76 H.G. B.E. 11-23-76	
R2	CHG. TITLE	8-18-70 H.G. H.G.	DL
R1	CHANGED TITLE	5-6-65 H.G.	R.E.B.

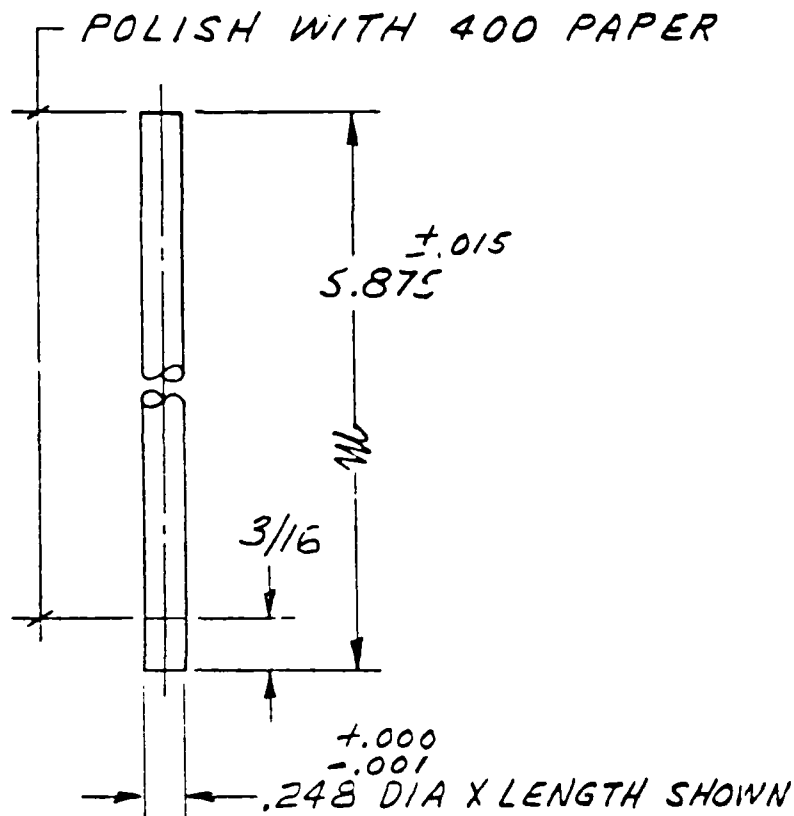
STANFORD LINEAR ACCELERATOR—M U.S. ATOMIC ENERGY COMMISSION		TITLE TUBE, PUMPOUT XK-5 KLYSTRON	
MAT'L. 1 1/4 O.D. X 1/16 W. CERT. O.F.H.G. CU		DATE 3-12-63	
ENGR. MERDINIAN CHK'D H.G.		SCALE 1"=1"	
DFTS GREENHILL 3-8-63 APP'D Melan		PF-700-655-01-R5	



1. MADE FROM PF-700-301-03
2. STRESS RELIEVE AT 950-1000°C. FOR 10-20 MIN. WITH FAST COOL
3. USE ONLY SLAC APPROVED MACHINING FLUID PER 5C-700-566-47

ITEM NO	PREFIX	BASE	SUFFIX	TITLE OR DESCRIPTION	QTY
	STOCK OR PART NO				
SCALE 1" = 1"		DO NOT SCALE DRAWING		NEXT ASSEMBLY: 5A-700-77C-01	
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ARE AS FOLLOWS: FRACTIONS .005 DECIMALS .005 ANGLES ALL NUMBERS		STAMFORD LINEAR ACCELERATION CENTER U.S. DEPARTMENT OF ENERGETICS STAMFORD UNIVERSITY STAMFORD CONNECTICUT		HOUSING, ANODE	
		STOCK # 8-68554888 PART # H. GREENHILL C-28 APPROVALS [Signature]		XK-5 KLYSTRON	
43 ALL NUMBERS				PF-700-682-01-F:5	

518310



NOTE:

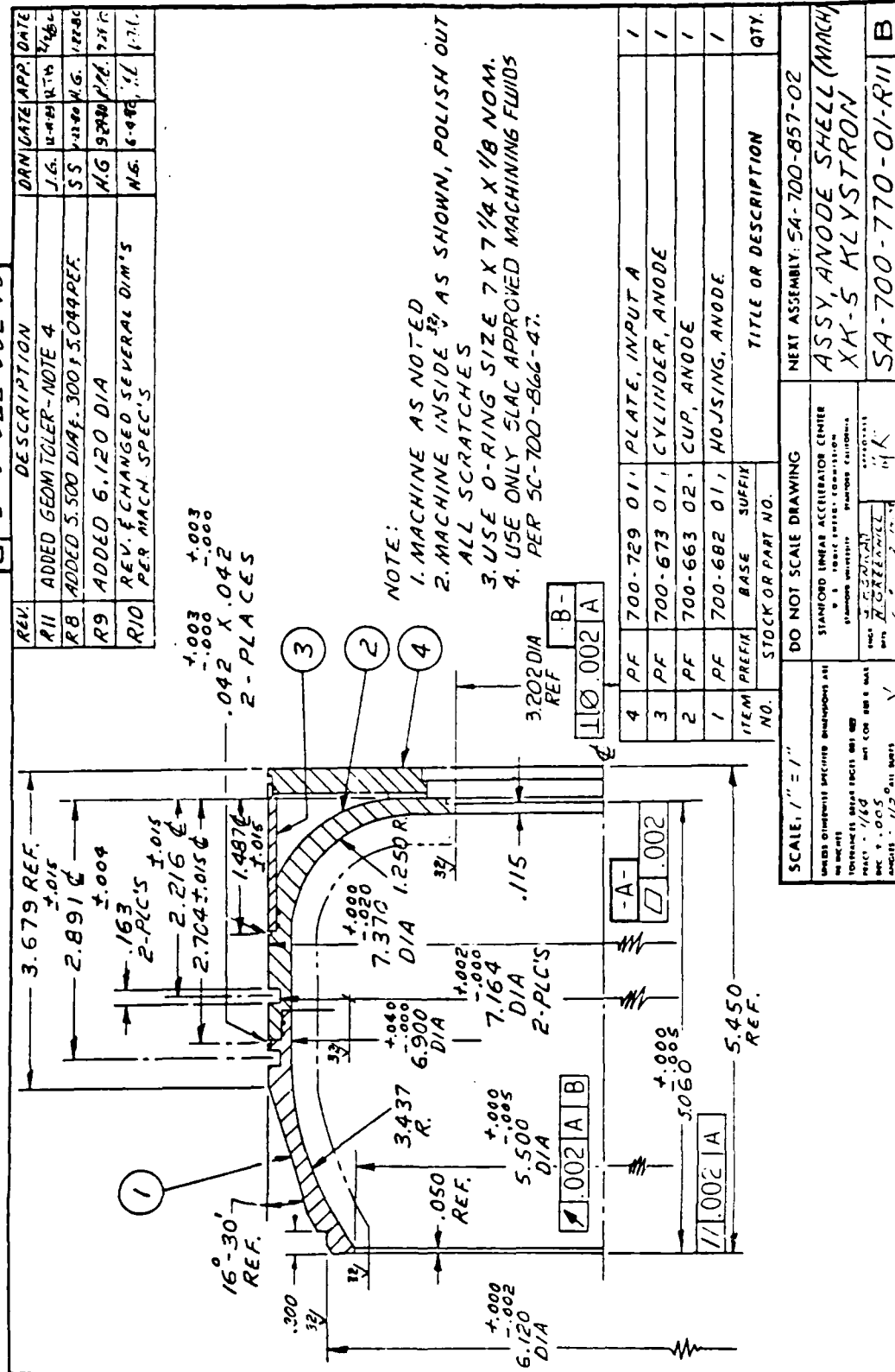
1. MAT'L: 1/4 DIA 304 L STN STL ROD
2. USE ONLY SLAC APPROVED MACHINING FLUIDS PER SC-700-866-47
3. NEXT ASSY: SA-700-783-01

UNLESS NOTED  
TOLERANCES: DECIMALS, FRACTIONS, ANGLES, RADI  
BRAIN CORNER .005  
INT. RADIUS .005  
DEC. .005  
ANGLES .125°  
32 MACH. SURF'S

R6	3/16 WAS 5/16 & 5.875 WAS 6.000	3-21-80 S.S.	3-21-80 H.G.
R5	ADDED POLISH NOTE	2-1-80 H.G.	H.K.
R4	CHG. TITLE	11-15-76 B.F.	1-7 K
R3	ADDED .248 DIA X 5/16 LG.	5-28-71 H.G.	110
R2	CHG. TITLE	6-18-70 H.G.	110
R7	ADDED NOTES 2 & 3	12-14-33 H.G.	2-3-84 P-16

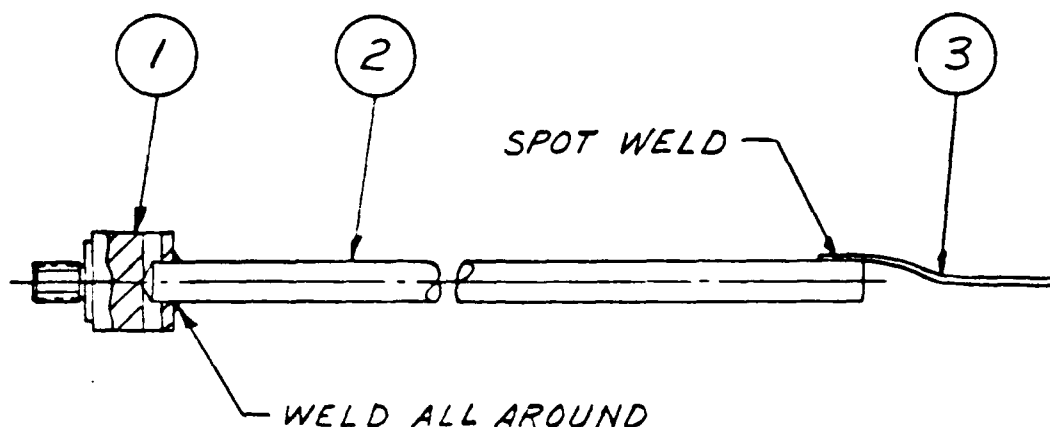
STANFORD LINEAR ACCELERATOR U.S. ATOMIC ENERGY COMMISSION		TITLE ROD. CENTER HEATER XK-5 KLYSTRON	
ENGR G. GREENHILL	CHK'D H.K.	DATE 2-22-66	SCALE 1" = 1" PF-700-759-01-R7
DFTS H. GREENHILL	APP'D		

MP-7



110114

PROPRIETARY DATA OF STANFORD UNIVERSITY AND/OR U. S. ATOMIC ENERGY COMMISSION  
RECIPIENT SHALL NOT PUBLISH THE WITHIN INFORMATION WITHOUT SPECIFIC PERMISSION  
OF STANFORD UNIVERSITY.

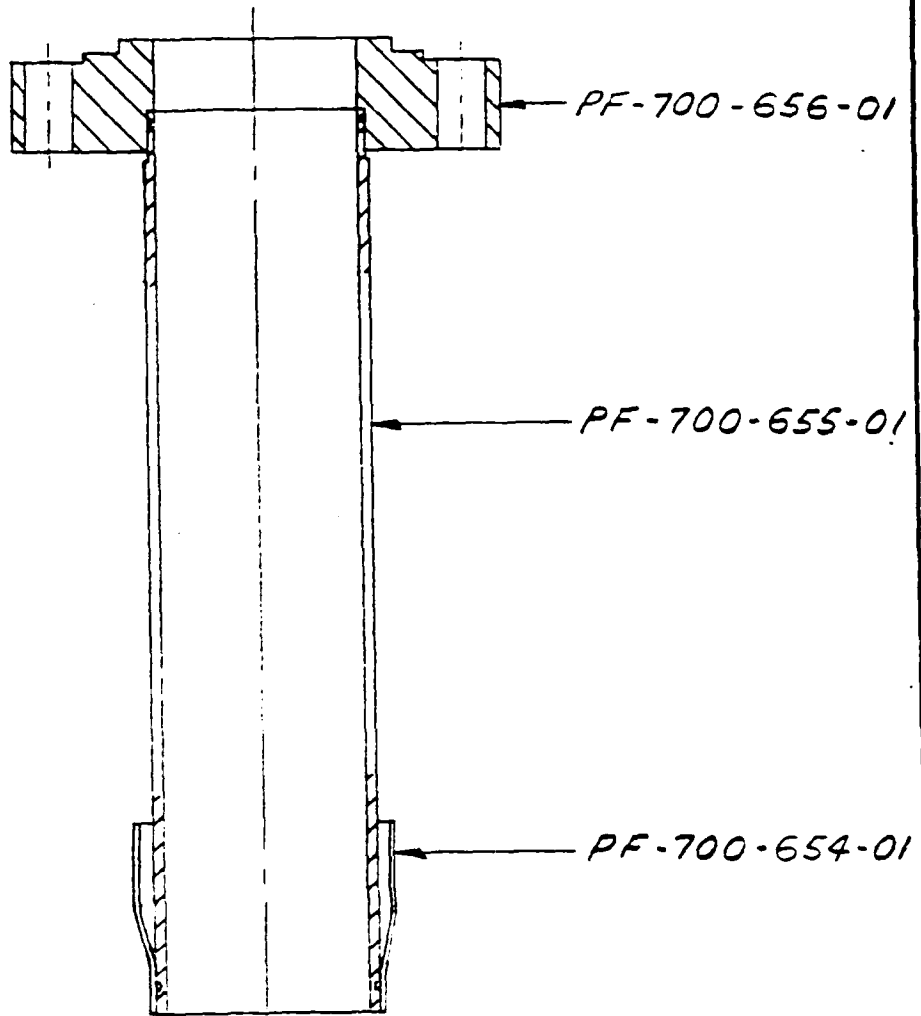


NOTE:

1. NEXT ASSY: SA-700-786-01

3				.005 THK. X. 300X1.5 LG. NICKEL STRIP	4		
2	PF	700-759	01	ROD, CENTER HEATER	1		
1	PF	700-229	01	CYLINDER	1		
ITEM NO.	PREFIX	BASE	SUFF.	DESCRIPTION	QTY.		
REV.	DESCRIPTION			DRN.	DATE	APP.	DATE
R1	CHG. TITLE			H.G.	8-19-70	FJC	8-5-70
R2	CHG. TITLE			B.E.	11-15-70	ATK	11-15-70
R3	.300 WAS .287			S.S.	5-12-71	H.G.	6-11-71
R4	ADDED NOTE 1.			H.G.	12/14/73	RTG	2/2/74
STANFORD LINEAR ACCELERATOR CENTER U. S. ATOMIC ENERGY COMMISSION STANFORD UNIVERSITY STANFORD, CALIFORNIA				ASM. CTR. HEATER COND. XK-5 KLYSTRON			
ENGR. R. CALLIN	APPROVALS			SA-700-783-01-R4			
DPTS. H. GREENHILL	1-3-69			A			
CHE. L. L.							

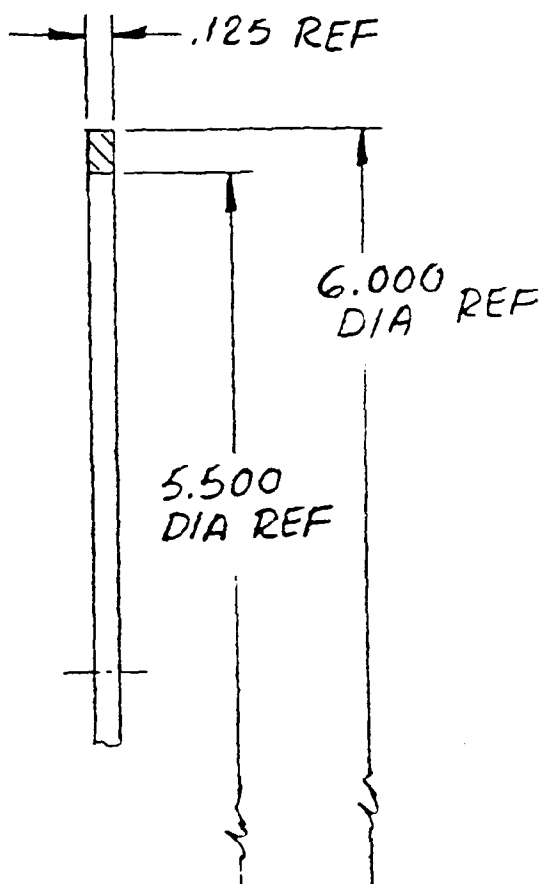
PROPRIETARY DATA OF STANFORD UNIVERSITY AND/OR U. S. ENERGY RESEARCH AND DEVELOPMENT ADMINISTRATION  
 RECIPIENT SHALL NOT PUBLISH THE WITHIN INFORMATION WITHOUT SPECIFIC PERMISSION OF STANFORD UNIVERSITY



SCALE: 1" = 1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
14 JUL 1973					
STANFORD LINEAR ACCELERATOR CENTER U.S. ENERGY RESEARCH AND DEVELOPMENT ADMINISTRATION STANFORD UNIVERSITY STANFORD, CALIFORNIA		ASSY, PUMPOUT XK-5 KLYSTRON			
ENGR <u>G. KONRAD</u> DITS <u>H. GREENHILL</u> CNE <u>CPA 7-12-73</u>	APPROVALS <u>[Signature]</u>	SA-700-857-17-R0		A	

AND/OR U.S. DEPARTMENT OF ENERGY  
 INFORMATION WITHOUT SPECIFIC  
 PERMISSION OF STANFORD UNIVERSITY



NOTE:

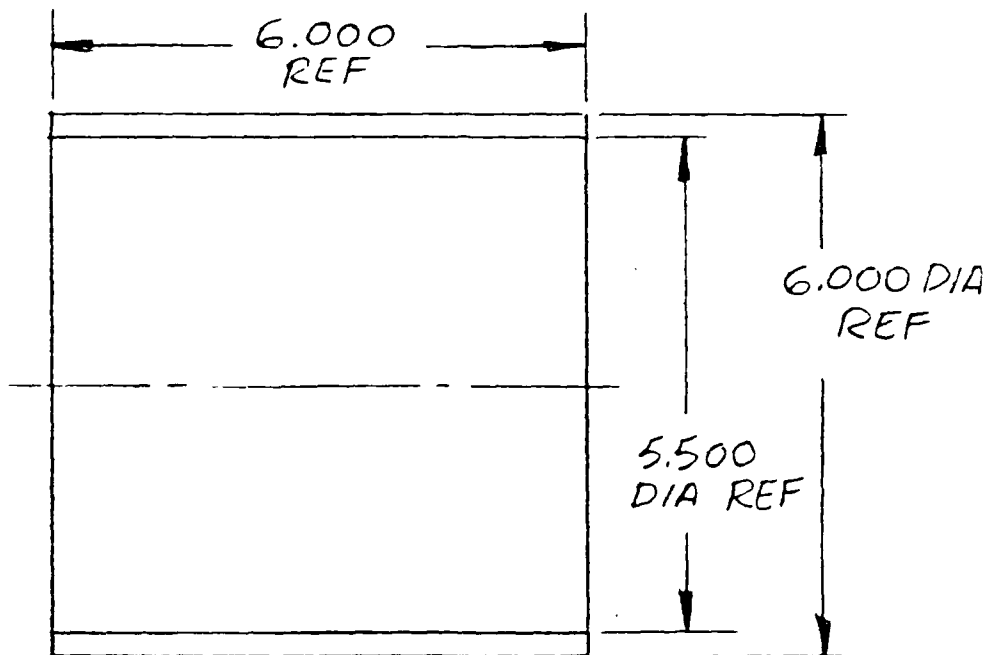
1. MADE FROM PF-700-648-01
2. OFHC Cu. PLATE 0.0002 ALL METALLIZED SURFACES.

SCALE: 1"=1"

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
STANFORD LINEAR ACCELERATOR CENTER U.S. DEPARTMENT OF ENERGY STANFORD UNIVERSITY STANFORD, CALIFORNIA		RING, PL - BACK UP XK-5 KLYSTRON			
ENGR. <u>P. BOESENBERG</u> DFTS <u>M. WALLACE</u> CHR <u>H.E.</u>	APPROVALS <u>[Signature]</u> 2-24-82	PF-700-862-04-R0		<b>A</b>	

AND/OR U.S. DEPARTMENT OF ENERGY  
INFORMATION WITHOUT SPECIFIC

PROPRIETARY DATA OF STANFORD UNIVERSITY  
RECIPIENT SHALL NOT PUBLISH THE WHI  
PERMISSION OF STANFORD UNIVERSITY



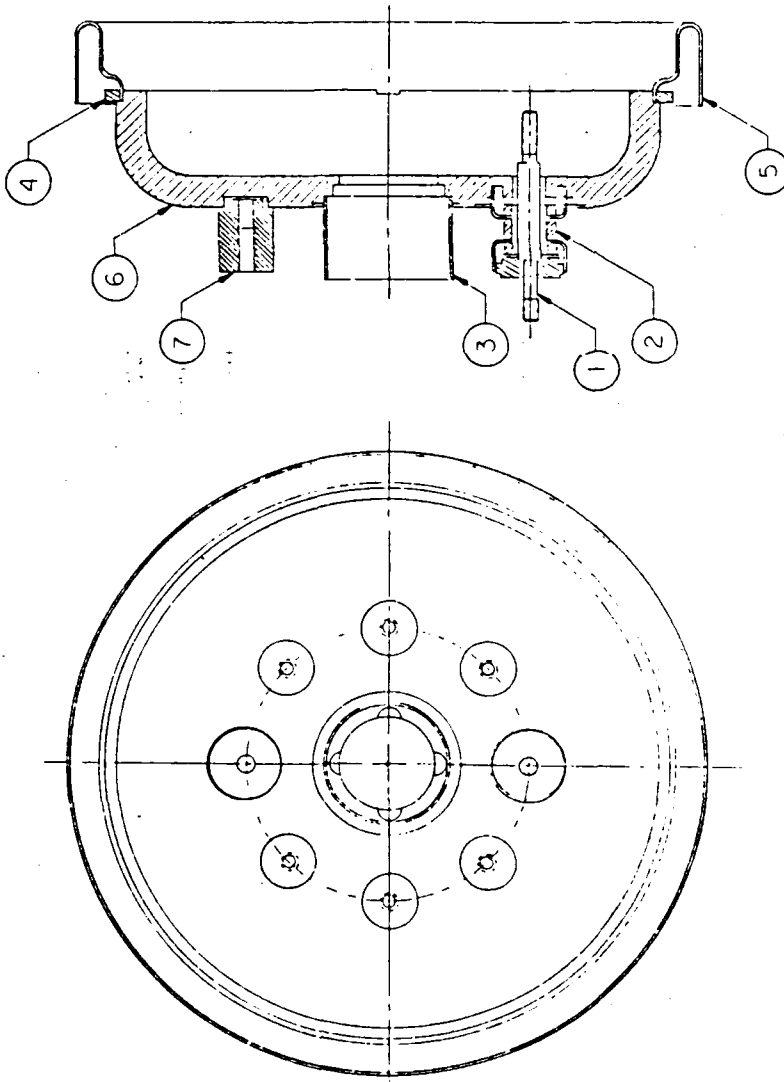
NOTE:

1. MADE FROM PF-700-649-01
2. OFHC C4. PLATE 0.0002 ALL METALLIZED SURFACES

SCALE:  $\frac{1}{2}'' = 1''$

REV.	DESCRIPTION	DRN.	DATE	APP.	DATE
<b>STANFORD LINEAR ACCELERATOR CENTER</b> U.S. DEPARTMENT OF ENERGY STANFORD UNIVERSITY STANFORD, CALIFORNIA		<b>CERAMIC, PLATED</b> <b>XK-5 KLYSTRON</b>			
ENGR. <u>R. BOESENBERG</u>	APPROVALS <i>[Signature]</i> 2-24-82		<b>PF-700-862-05-R0</b>		<b>A</b>
DFTS <u>M. WALLACE</u>					
CHK <u>H. G.</u>					





NOTE:  
1. ALL BRAZING TO BE NICKEL.

A55

REV	DESCRIPTION	DRN	DATE	APP	DATE
R1	REDRAWN WITH PARTS LIST - SAME DIMS AS JG	JG	11/18/53		11/18/53

ITEM NO	PREFIX	BASE	SUFFIX	TITLE OR DESCRIPTION	QTY
7	PF	700-638	CI	CATHODE STUD	6
6	PF	700-288	CI	CUP BASE - FINISHED	1
5	PF	700-226	CI	TAKE APART JOINT	1
4	PF	700-227	CI	RING, REINFORCING	1
3	PF	700-224	CI	SEALING RING - R.O.T. - FEMALE	1
2	SA	700-851	74	ASSEMBLY CUPS AND INSULATORS	2
1	SA	700-851	73	ASSEMBLY ROD - CYLINDER - FEED THRU	2

UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES		SCALE: 1/1		DO NOT SCALE DRAWING	
TOLERANCES: BREAK EDGES .003 - .015 INTERNAL CORNERS .015 R MAX FRACTIONS 1/16 DEC 1/1000		STANFORD LINEAR ACCELERATOR CENTER S 3 DEPARTMENT OF PHYSICS STANFORD UNIVERSITY STANFORD, CALIFORNIA		NEXT ASSEMBLY: AD-704-011-00	
APPROVALS: INCH J.G. JG BY J.G. JG CHKD J.G. JG		DATE: 11/18/53		ASSEMBLY, BASE CUP XK-5 KLYSTRON	
ANGLES: ALL SHARP		SA		700-857-01-R1	
		SH 1 OF 1		C	

SA-700-857-01-R1

APPENDIX A-4

PARTS AND MATERIALS LIST

10 FIN-RA001 ALDAMA										ENGINEERING INDENTED EXPLOSION										FEB 6, 1986 MDAY 793										PAGE 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APPENDIX E

"ELECTRON GUN BREAKDOWN"

by

Dr. Armand Stagnans, Varian Associates, Inc.

1985 High-Voltage Workshop

February 26, 1985

Monterey, California



**ELECTRON GUN BREAKDOWN**  
**ARMAND STAPRANS**  
**VARIAN ASSOCIATES, INC.**

PRESENTED AT THE  
1985 HIGH-VOLTAGE WORKSHOP  
FEBRUARY 26, 1985  
MONTEREY, CALIFORNIA

## Electron Gun Breakdown

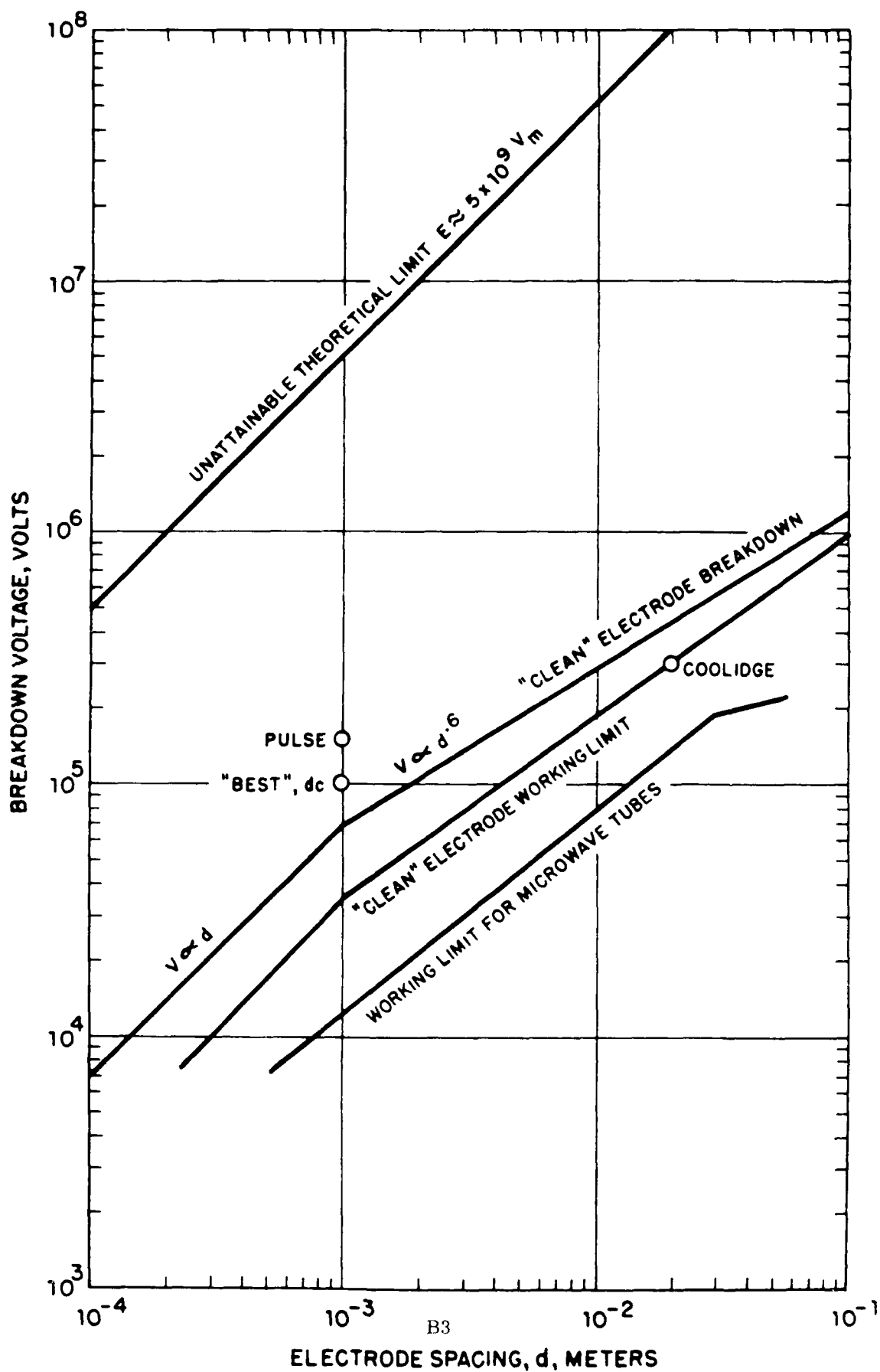
A. Staprans  
Varian Associates Inc.  
611 Hansen Way  
Palo Alto, CA 94303

The electron gun is usually the portion of a microwave tube that is most stressed by high voltage and is frequently subject to breakdown. This is a consequence of design constraints which often require the use of close-spaced vacuum gaps between gun electrodes.

The design criteria for voltage hold-off in guns are reviewed. Largely because of the presence of evaporation from a hot cathode, the acceptable safe voltage between gun electrodes is substantially lower than for a similarly spaced "clean" vacuum gap. Design guidelines for achieving adequate voltage hold-off in guns are discussed, including allowable gradients, electrode spacings, pulse vs dc operation, electrode materials, and insulator configurations.

The tube-power supply interface plays a very important role in minimizing gun breakdown. Arc energy limiting means such as crow-bars and arc current limiting impedances are discussed and design criteria suggested.

# VACUUM GAP VOLTAGE BREAKDOWN COMPARISON





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## **SPECIAL FACTORS IN ELECTRON GUN BREAKDOWN**

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- PRESENCE OF A HOT CATHODE — BARIUM DEPOSITION ON ELECTRODES
- “LOW” IMPEDANCE POWER SUPPLIES — LARGE AVAILABLE ARC ENERGY
- ELEVATED ELECTRODE TEMPERATURES — ENHANCED FIELD EMISSION
- LARGE ELECTRODE AREA (COMPARED TO SPACING)
- COMPLEX ELECTRODE SHAPES — DIFFERENT FROM SIMPLE GAP THEORIES
- PRESENCE OF MAGNETIC FIELD — AFFECTS CHARGED PARTICLE PATHS
- LIMITED CHOICE OF MATERIALS



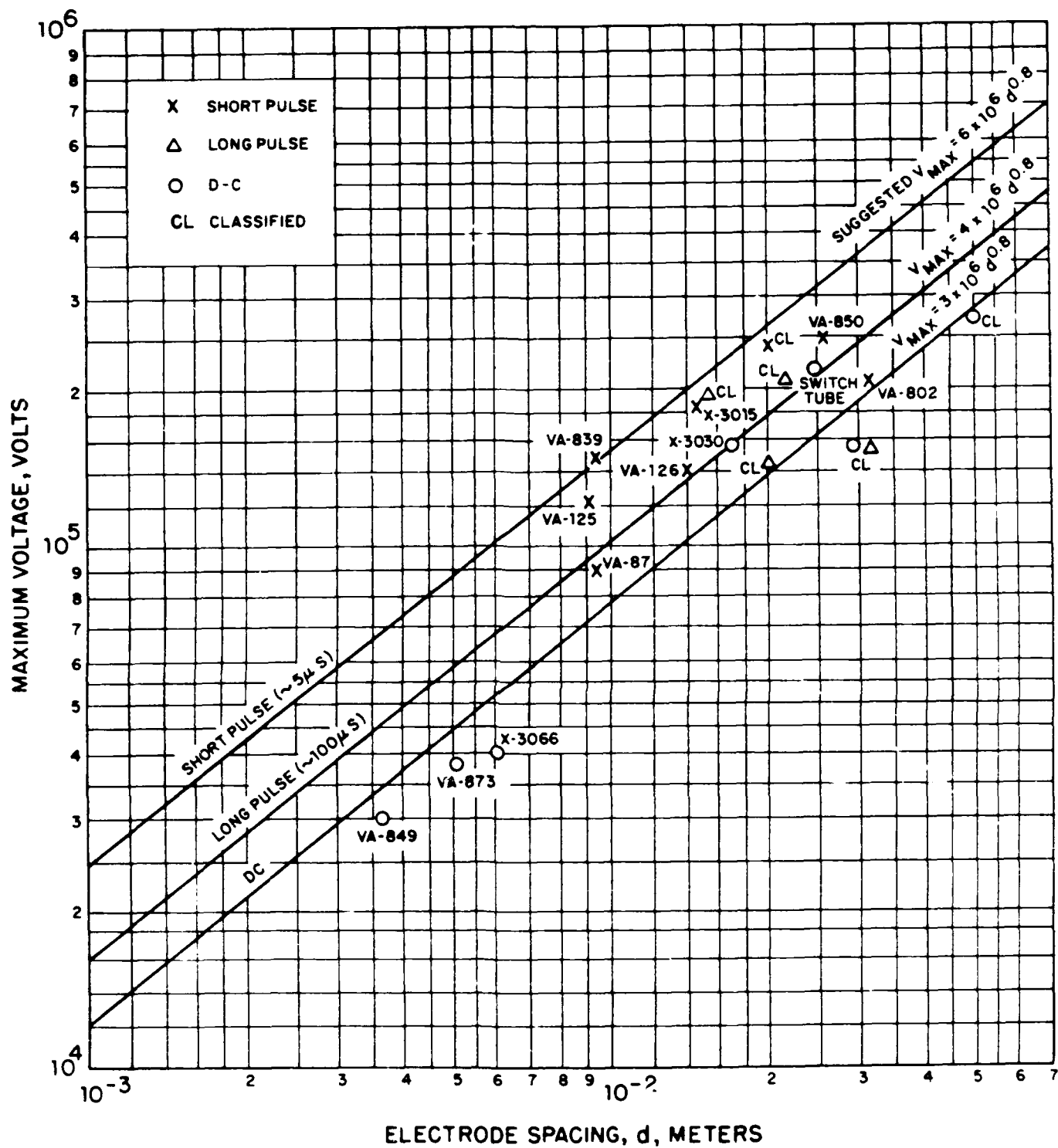


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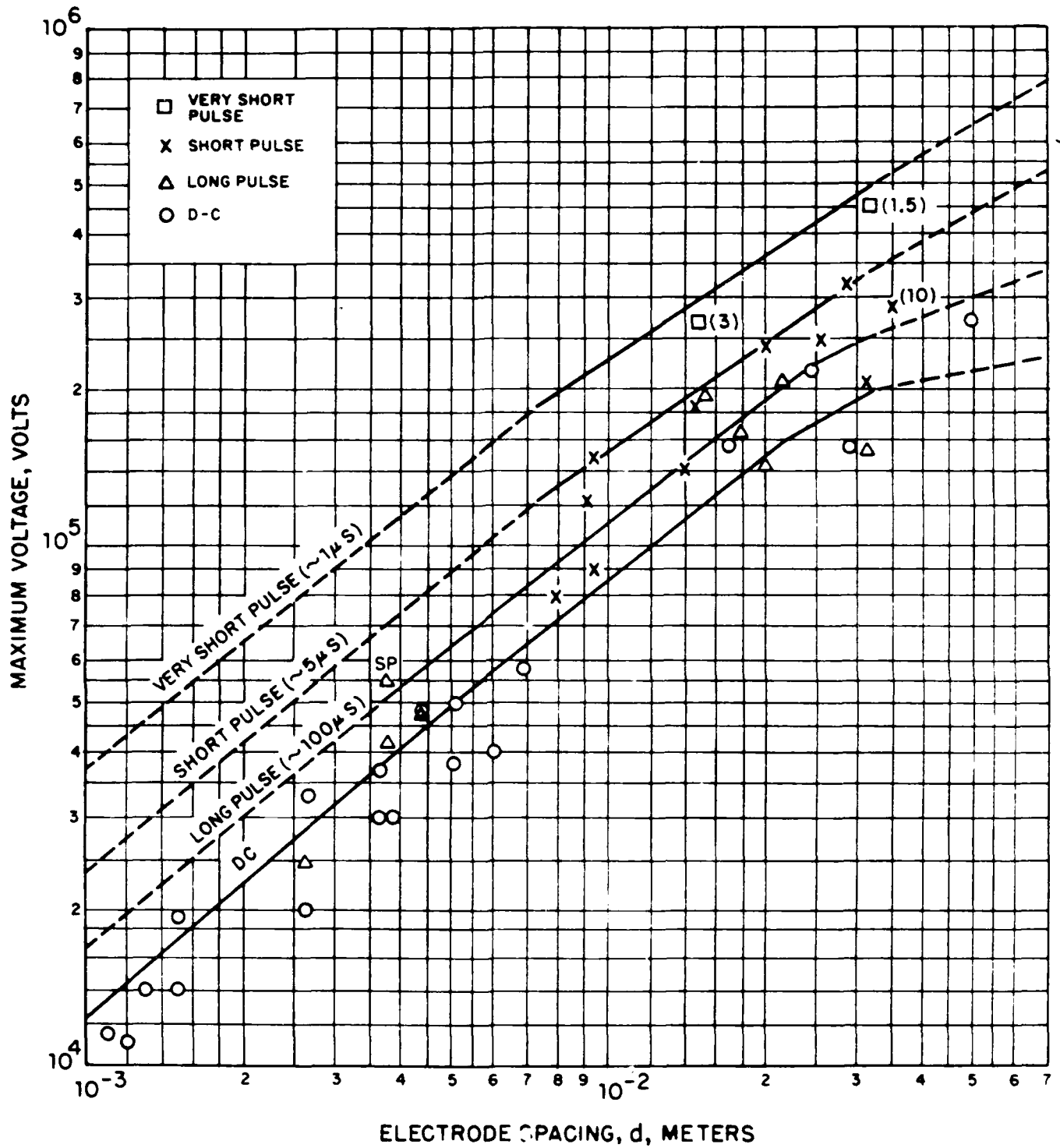
## **ELECTRODE SPACING RATHER THAN GAP FIELD IS PREFERRED VARIABLE**

- FIELD AT ELECTRODE SURFACE IS BUT ONE OF MANY FACTORS AFFECTING BREAKDOWN. ELECTRODE SHAPES AND SIZES ARE ALSO IMPORTANT. MINIMUM SPACING IS A GENERAL PARAMETER.
- FOR WELL DESIGNED GUN FOCUS ELECTRODES, FIELD ENHANCEMENT FACTOR ABOVE  $V/d$  IS LOW:  
USUAL RANGE 1.3 to 1.7  
AVERAGE 1.5
- ELECTRODE SPACING DATA IS MORE AVAILABLE THAN GRADIENTS
- EXISTING DATA YIELDS FAIRLY CONSISTENT RESULTS
- CONVENIENT DESIGN PARAMETER

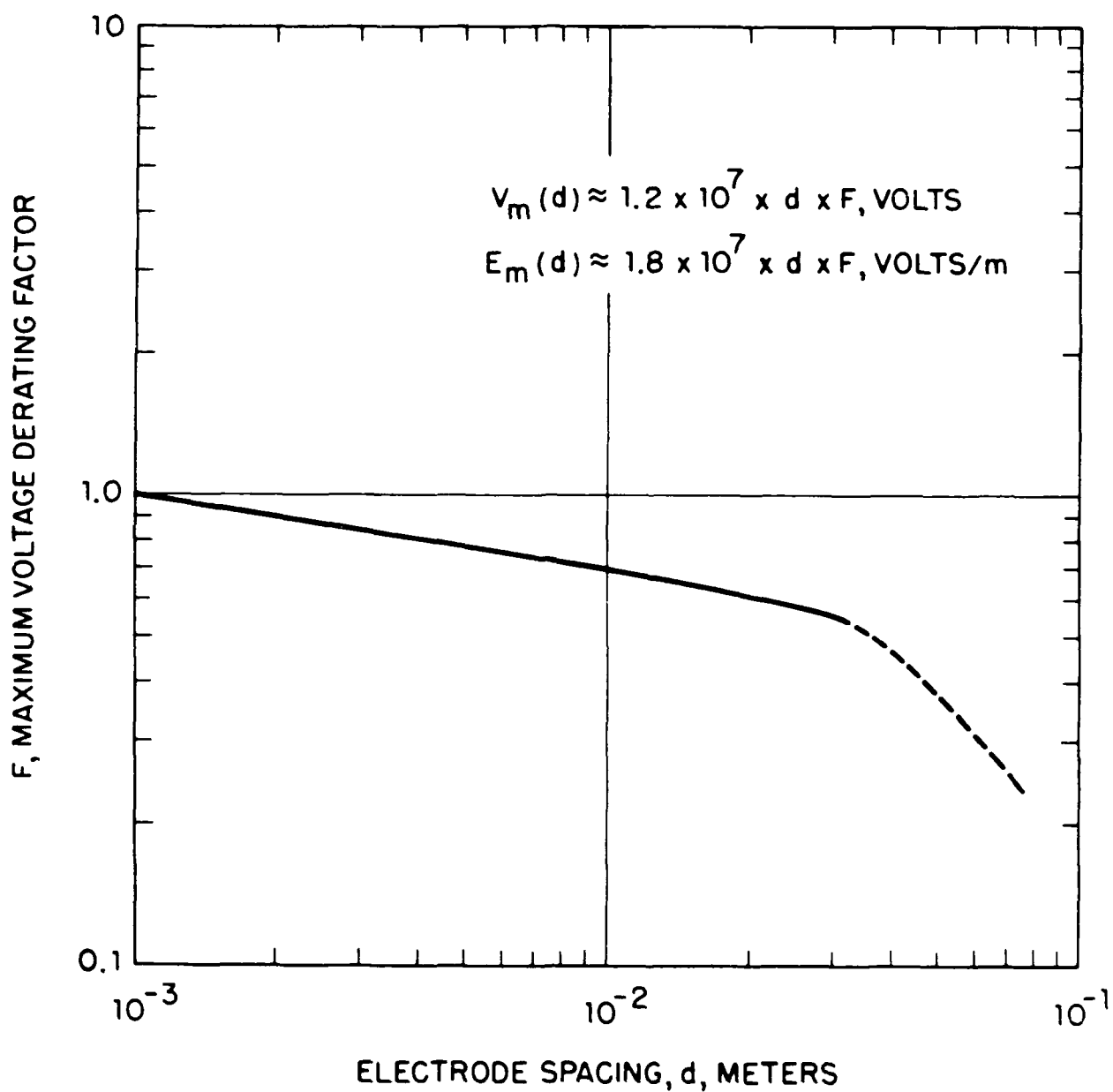
# GUIDE TO HV SPACING DESIGN IN ELECTRON GUNS (1966)



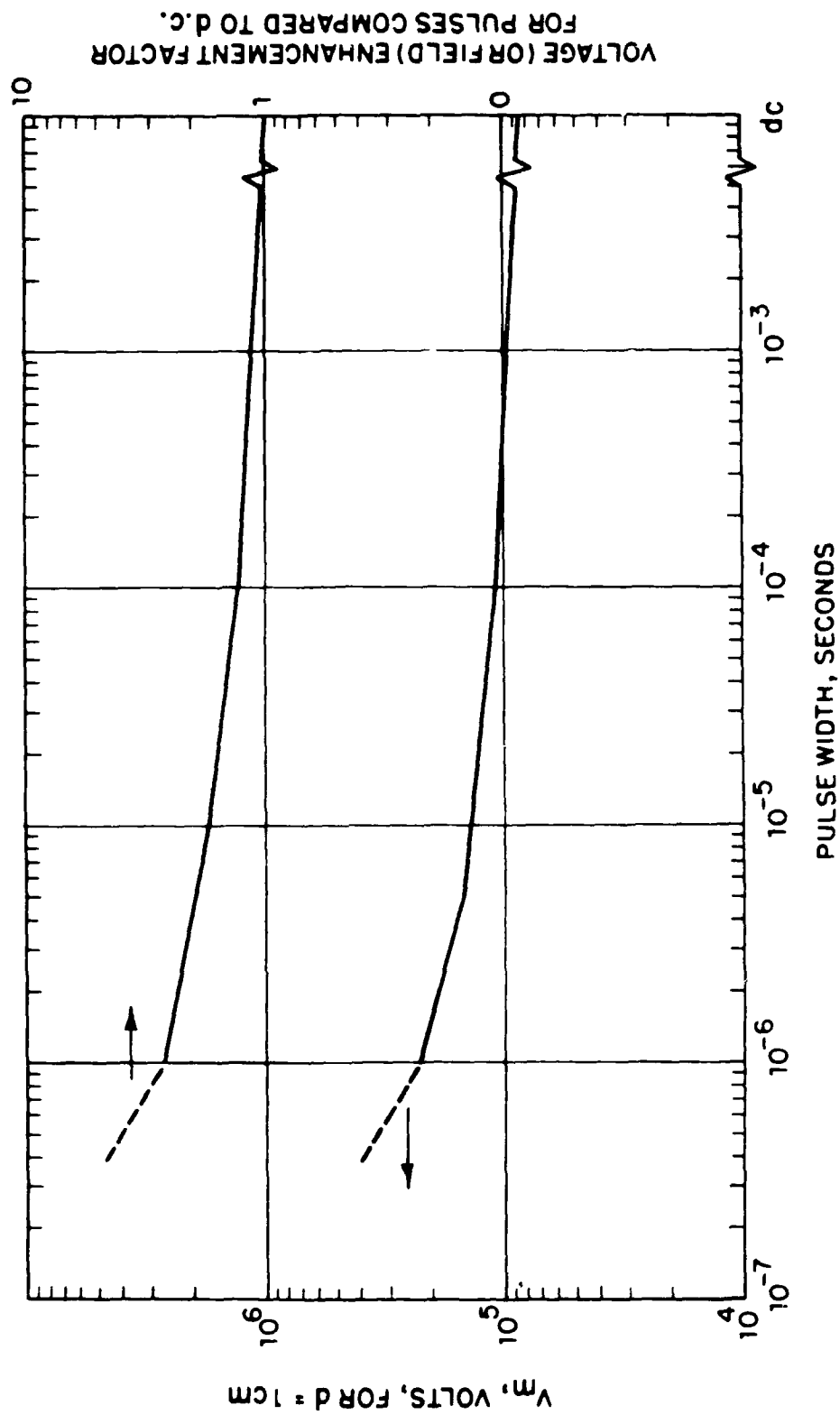
# GUIDE TO HV SPACING DESIGN IN ELECTRON GUNS (1985)



MAXIMUM DESIGN VOLTAGE,  $V_m$ , OR FIELD,  $E_m$ ,  
DERATING FACTOR,  $F$ , FOR ELECTRODE SPACINGS  
ABOVE 1 mm FOR d.c. CONDITIONS



# MAXIMUM DESIGN VOLTAGE, $V_m$ , vs. PULSE WIDTH





## SUMMARY OF DESIGN CRITERIA

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- CURVES OF MAXIMUM VOLTAGE vs ELECTRODE SPACING FOR PULSE AND DC
- ALTERNATELY, FOR MORE APPROXIMATE ESTIMATES AND PARAMETRIC CALCULATIONS, FOR GAPS UP TO ABOUT 3 cm, THE FOLLOWING APPLIES:

$$V_{\max} \approx K \times 10^6 d^{0.8}, \text{ where}$$

K	≈ 3	FOR DC
	≈ 4	FOR 100 msec PULSES
	≈ 6	FOR 5 msec PULSES
	≈ 9	FOR 1 msec PULSES



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## **ELECTRODE MATERIALS AND SURFACES**

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- FOR NEGATIVE (FOCUS) ELECTRODE, STAINLESS STEEL (SOMETIMES OXIDIZED) IS COMMON USAGE. IRON AND MOLYBDENUM ARE ALTERNATES. COPPER IS STILL USED FOR THE LOWER VOLTAGES.
- COPPER, STAINLESS STEEL AND IRON ARE USUAL ANODE MATERIALS, BUT STAINLESS STEEL IS PREFERABLE.
- MECHANICAL POLISHING AND SUBSEQUENT CLEANING IS PREFERRED, BUT CARE MUST BE TAKEN TO PREVENT SURFACE CONTAMINATION.
- MICROSCOPIC PROPERTIES OF SURFACES ARE IMPORTANT.



## **GUN INSULATOR ISSUES**

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- **SURFACE BREAKDOWN CAN OCCUR FROM ELECTRON EMISSION FROM THE TRIPLE JUNCTION AND SECONDARY ELECTRON MULTIPLICATION AND CHARGING, OR FROM SURFACE CONTAMINATION/LEAKAGE.**
- **DESIGN CRITERIA FOR CERAMIC INSULATORS:  
LENGTH  $\sim 10 \times$  THAT OF EQUIVALENT VACUUM GAP  
WALL THICKNESS TO WITHSTAND FULL APPLIED VOLTAGE  
GROOVED OR ROUGHENED VACUUM SIDE SURFACES  
SHIELDING FROM CATHODE, ARC, AND BEAM HEATING  
EVAPORANTS  
CORONA SHIELDS FOR TRIPLE JUNCTIONS  
FIELD CONCENTRATION, IF ANY, ON NEGATIVE END OF  
INSULATOR**





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## ARC CHARACTERISTICS AND PROTECTION CRITERIA

- BUILDUP TIME IS SHORT — TEN(S) OF NANoseconds
- SUBSEQUENT METAL VAPOR ARC DROP IS LOW — ABOUT 20 VOLTS
- ELECTRODE AND LEAD/BUSWORK STORED ENERGY IS ALWAYS AVAILABLE TO THE ARC (BUILDUP) — USUALLY LESS THAN 1 JOULE
- SUBSEQUENT ARC DISSIPATION SHOULD BE LIMITED TO A COMPARABLE VALUE,  $\sim 1$  JOULE, BY PROTECTIVE CIRCUITRY
- COMMON TUBE SPECIFICATION REQUIREMENTS OF LARGER ARC ENERGIES, E.G. 40 JOULES, ARE UNREALISTIC AND ONLY FUNCTION BECAUSE ONLY A SMALL FRACTION OF THIS ENERGY IS DISSIPATED IN THE ARC



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## RECOMMENDED MEASURES FOR ~ 1 JOULE DISSIPATION

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- KEEP ELECTRODE AND LEAD/BUSWORK CAPACITANCES LOW
- IF POSSIBLE, "ISOLATE" POWER SUPPLY FROM GUN BY PROVIDING A TIME CONSTANT MUCH LARGER THAN ARC BUILDUP TIME
- FOR UP TO ABOUT 20 KV, A 50 TO 100  $\Omega$  SERIES RESISTOR, AND ARC CURRENT LIMITATION TO ABOUT 100 A IS ADEQUATE
- FOR VOLTAGES ABOVE ABOUT 40 KV, AN ELECTRONIC CROWBAR IS USUALLY NECESSARY, ITS SPEED DEPENDENT UPON CURRENT. LIMITING CHARACTERISTICS OF THE SUPPLY:
  - 100 A MAX  $\rightarrow$  0.5 msec CROWBAR
  - 10,000 A MAX  $\rightarrow$  5  $\mu$ sec CROWBAR



## SUMMARY

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- NO SIGNIFICANT IMPROVEMENTS IN GUN VOLTAGE CAPABILITY IN THE LAST 20 YEARS, BUT:
- SIGNIFICANTLY BETTER UNDERSTANDING OF VACUUM ARCS EXISTS
- DESIGN LIMITS AND TECHNIQUES ARE BETTER UNDERSTOOD
- PROTECTIVE CIRCUITS ARE BETTER UNDERSTOOD AND ACCEPTED



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## ACKNOWLEDGEMENT

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MOST OF THE ELECTRON GUN DATA USED WAS OBTAINED FROM:

VARIAN MICROWAVE TUBE DIVISION

VARIAN BEVERLY MICROWAVE DIVISION

STANFORD LINEAR ACCELERATOR CENTER (G. KONRAD)

LITTON ELECTRON DEVICES (R. TRUE)